# **SOIL-MAT ENGINEERS & CONSULTANTS LTD.**

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August 15, 2018

PROJECT No.: SM 188337-G

HALDIMAND COUNTY – ENGINEERING DIVISION 3-100 Haddington Street Caledonia, Ontario N3W 2N4

Attention: Lloyd Rollinson Project Manager

GEOTECHNICAL INVESTIGATION
PROPOSED INTERSECTION IMPROVEMENTS
ARGYLE STREET SOUTH
CALEDONIA, ONTARIO

Dear Mr. Rollinson,

Further to your authorisation, SOIL-MAT ENGINEERS & CONSULTANTS LTD. has completed the fieldwork and laboratory testing, and report preparation in connection with the above noted project. The investigation and reporting were undertaken in general accordance with our proposal P7375, dated May 2, 2018 and revised May 28, 2018. Our comments and recommendations, based on our findings at the ten [10] borehole locations are presented herein.

#### 1. INTRODUCTION

We understand that the project will involve improvements to the intersection of Argyle Street South and Haddington Street, as well as sanitary sewer replacement along Argyle Street from approximately Kinross Street, to Forfar Street in Caledonia, Ontario. The purpose of this geotechnical investigation work was to assess the subsurface soil conditions, and to provide our comments and recommendations with respect to the design and construction of the proposed improvements, from a geotechnical point of view.

This report is based on the above summarised project description, and on the assumption that the design and construction will be performed in accordance with applicable codes and standards. Any significant deviations from the proposed project design may void the recommendations given in this report. If significant changes are made to the proposed design, this office must be consulted to review the new design

with respect to the findings of this investigation. It is noted that, other than limited background testing detailed below, the information contained in this report does not

#### 2. PROCEDURE

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reflect upon the environmental aspects of the site.

A total of ten [10] sampled boreholes were advanced at the locations illustrated in the attached Drawing Nos. 1 and 2, Borehole Location Plans. The boreholes were advanced using continuous flight power auger equipment on June 22, 2018 under the direction and supervision of a representative of SOIL-MAT ENGINEERS, to termination at depths of approximately 0.9 to 6.7 metres beneath the existing road surface. Upon completion of drilling all of the boreholes were backfilled in general accordance with Ontario Regulation 903, and the pavement surfaces reinstated with a pre-mixed asphaltic concrete 'cold patch' product.

Representative samples of the subsoils were recovered from the borings at selected depth intervals using split barrel sampling equipment driven in accordance with the requirements of the ASTM test specification D1586, Standard Penetration Resistance Testing. After undergoing a general field examination, the soil samples were preserved and transported to the SOIL-MAT laboratory for visual, tactile, and olfactory classifications. Routine moisture content tests were performed on all soil samples recovered from the borings, with hand penetrometer testing conducted on select cohesive samples.

In addition, twenty-one [21] selected samples were submitted for background analytical testing, in general accordance with the requirements set out in the RFQ document and subsequent emails. The samples were submitted to ALS Environmental, an accredited Canadian Environmental Laboratory for analytical testing for a standard panel of metal and inorganic parameters for comparison to the <u>Soil</u>, <u>Ground Water and Sediment Standards</u> for Use Under Part XV.1 of the *Environmental Protection Act*. The results of this testing can be found appended to the end of this report.

The boreholes were located in the field by a representative of SOIL-MAT ENGINEERS & CONSULTANTS LTD., in general accordance with the drawings provided to our office by Haldimand County. The ground surface elevation at the borehole locations has been referenced to the existing road surface.

Details of the conditions encountered in the boreholes, together with the results of the field and laboratory tests, are presented in Log of Borehole Nos. 1 through 10, inclusive, following the text of this report. It is noted that the boundaries of soil types indicated on

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the borehole logs are inferred from non-continuous soil sampling and observations made during drilling. These boundaries are intended to reflect transition zones for the purpose of geotechnical design and therefore should not be construed as the exact planes of geological change.

## 3. SITE DESCRIPTION AND SUBSURFACE CONDITIONS

The project area consists of the section of Argyle Street from Haddington Street to Wigton Street in Caledonia, Ontario. The roadway is a three lane asphaltic concrete paved urban cross section with concrete curbs and catch basins. The roadway serves both commercial and residential properties, with moderate to heavy vehicle traffic. The pavement surface was noted to be in a relatively fair to poor condition with areas of frequent longitudinal, transverse, and alligator cracking, as well as occasional repair patches.

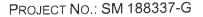
The subsurface conditions encountered at the borehole locations are summarised as follows:

#### Topsoil

A surficial veneer of topsoil approximately 300 millimetres in thickness was encountered at Borehole No. 3, which was advanced south of the intersection of Argyle Street or Haddington Street. It is noted that the depth of topsoil may vary significantly across the site from the depth encountered at this single borehole location. It is also noted that the term 'topsoil' has been used from a geotechnical point of view, and does not necessarily reflect its nutrient content or ability to support plant life.

#### **Pavement Structure**

Borehole No. 1 was advanced through the granular pavement structure of the gravel driveway north of the intersection, which was found to consist of approximately 300 millimeters of granular materials. Borehole No. 4 was advanced through the pavement of Haddington Street, while all boreholes other than Borehole Nos. 1, 3, and 4 were advanced through the existing pavement structure of Argyle Street. The pavement structure on these roadways was found to consist of approximately 100 to 380 millimetres of asphaltic concrete overlying 300 to 600 millimetres of compact granular base, summarised as follows:





Borehole No.	1	2	4	5	6	7	8	9	10
Asphaltic Concrete (mm)	N/A	380	100	100	200	300	200	300	200
Granular Base (mm)	300	400	600	600	600	600	600	600	600

#### Sand and Gravel Fill

A deposit of sand and gravel fill was encountered beneath the pavement structure at Borehole No. 10. The course granular material was brown to grey in colour and was noted to be in a compact state. It is noted that the amount of crushed limestone bedrock aggregate encountered made the transition from granular base materials of the pavement structure to the sand and gravel fill deposit somewhat indistinct. The sand and gravel fill deposit was proven to a depth of approximately 2.1 metres in Borehole No. 10.

#### Silty Clay

Native silty clay was encountered beneath the pavement structure or topsoil at all borehole locations. The silty clay soils encountered were brown to greyish brown in colour, transitioning to grey at depths of approximately 3.5 to 5.0 metres below grade, contained trace to some gravel, and were generally firm to very stiff in consistency. The upper layers of the silty clay encountered in the boreholes had a 'reworked' appearance with occasional organic inclusions likely associated with grading activities during construction of the roadway, as well as having been subjected to ongoing traffic loads and freeze-thaw cycles. Silty clay was proven to termination at depths ranging from approximately 0.9 to 6.7 metres below the existing road surface at all borehole locations.

Grain size analyses were conducted on a total of two [2] selected samples, the results of which can be found appended to the end of this report, and are summarised as follows:

TABLE A
Grain Size Analyses

Sample ID	Depth	% Clay	% Silt	% Sand	% Gravel
BH4 SS4	2.8	70	26	4	0
BH9 SS3	1.8	58	39	3	0

Atterberg limits testing was also conducted on the same selected samples which were subjected to grain size analyses. The results of these analyses are presented in the attached Drawing No. 2, Atterberg Limits, and summarised as follows:

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# TABLE B Atterberg Limits

Sample ID	Approx. Depth [m]	Plastic Limit, w <sub>P</sub> [% moisture]	Liquid Limit. w <sub>L</sub> [% moisture]	Plasticity Index,
BH4 SS4	2.8	55.3	26.1	29.2
BH9 SS3	1.8	51.6	23.4	28.2

The field and laboratory testing demonstrate the silty clay deposit to be inorganic clays of medium to high plasticity. These soils are a highly cohesive material, with moderate plasticity, and very low permeability on the order of 10-8 cm/sec or lower.

#### **Groundwater Observations**

All boreholes were recorded as 'dry' upon completion of drilling. It is noted that insufficient time would have passed for the static groundwater level to stabilise in the open boreholes. However, in cohesive soils such as the silty clay encountered in the boreholes, the static groundwater level generally coincides with the transition in colour from brown to grey. As such, based on our observations during drilling and experience in the area, the static groundwater is estimated at depths on the order of perhaps 3 to 5 metres below the existing road surface.

#### 4. EXCAVATIONS

It is anticipated that the excavations for the proposed improvements and sanitary sewer replacement works will extend to depths of up to approximately 2 to 5 metres below the existing road surface. Excavations through surficial fill materials would be expected to remain stable at inclinations of up to 45 degrees to the horizontal. Excavations through the native silty clay should be relatively straightforward, with excavations remaining stable at inclinations of up to 60 degrees to the horizontal. Where wet seams are encountered, or during periods of extended precipitation, the sides of excavations should be expected to 'slough in' to as flat as 3 horizontal to 1 vertical, or flatter. Notwithstanding the foregoing, all excavations must comply with the requirements of the current Occupational Health and Safety Act and Regulations for Construction Projects. Excavation slopes steeper than those required in the Safety Act must be supported or a trench box must be provided, and a senior geotechnical engineer from this office should monitor the work.

Support of existing structures, underground services and roadways adjacent to the project area must also be considered in assessing the excavation support requirements. In this regard it is recommended that a pre-construction condition survey of the adjacent structures be conducted prior to the start of construction. It is anticipated that the majority of excavations for the proposed structure will be feasible as open cuts, as outlined above.

As noted above, the static groundwater level is estimated at depths of perhaps 3 to 5 metres, with some deeper excavations extending near to below this level. Some groundwater infiltration from permeable seams and from surface runoff should be expected. The rate of infiltration should be sufficiently low though the low permeability silty clay soils such that it should be readily controlled using conventional construction 'dewatering' techniques, such as pumping from sumps and ditches, even for excavations extending to or as much as 1 metre below the static groundwater level. Increased volumes of water should be anticipated when making connections to existing services. Surface water should be directed away from the excavations.

The base of the excavations in the silty clay encountered in the boreholes should remain firm and stable, however some localised instability may be experienced where excavations extend near the static groundwater level, or due to 'wet' seams, weather conditions, infiltration of groundwater, surface runoff, etc.. Excavation bases that experience localised base instability may require additional ballast stone, or other base stabilisation measures.

With firm and stable excavation base conditions, stabilised as required, standard pipe bedding material as specified by the Haldimand County or Ontario Provincial Standard Specification [OPSS] should be satisfactory. The bedding should be well compacted to provide sufficient support to the pipes and components (i.e. valve chambers, manholes etc.), and to minimise settlements of the roadway above the service trenches. Special attention should be paid to compaction under the pipe haunches.

Any utility poles, light poles, etc. located within 3 metres of the top of an excavation slope should be braced to ensure their stability. Likewise, temporary support might be required for other existing above and below ground structures, including existing underground services, depending on their proximity to the trench excavations.

#### 5. BACKFILL CONSIDERATIONS

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The majority of excavated materials will consist of the silty clay soils and granular fill materials, as encountered in the boreholes and described above. These materials are

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generally considered suitable for use as trench backfill, provided they are free of organic or otherwise deleterious materials. It is noted that the silty clay soils are not considered to be free draining, and will present some difficulty in achieving compaction in narrow trench excavations where access with compaction equipment is difficult. The sand and gravel fill materials may be acceptable for such applications, however this would be best Care should be taken ensuring sufficient assessed at the time of construction. compaction efforts, including necessary moisture conditioning, utilising appropriate equipment, thinner lifts, etc. are applied during compaction activities. Proper handling of the soils based on the material's moisture content and prevailing weather conditions during construction will be important to achieving a successful compaction operation. The silty clay soils encountered are generally considered to be wet of the standard Some moisture conditioning may be required Proctor optimum moisture content. depending upon weather conditions at the time of construction.

The native cohesive soils encountered are sensitive to moisture absorption and will become practically impossible to compact using conventional compaction equipment if they become wet/saturated during 'wet' weather. After a period of heavy precipitation, any near-surface wet or softened material should be allowed to air dry, or be removed and discarded.

Alternatively, the service trenches may be backfilled with a quality imported material. The use of a well-graded granular material, such as an OPSS Granular 'B' Type II (crushed bedrock) would be preferred, as it is less sensitive to moisture conditions and more readily compacted in the often restricted access areas of service trenches. Any imported fill should have its moisture content within 3 per cent of its optimum moisture content, conform to the project specifications with regards to material type and gradation, and meet the necessary environmental guidelines.

We note that where backfill material is placed near or slightly above its optimum moisture content, the potential for long term settlements due to the ingress of groundwater and collapse of the fill structure is reduced. Correspondingly, the shear strength of the 'wet' backfill material is also lowered, thereby reducing its ability to support construction traffic and therefore impacting roadway construction. If the soil is well 'dry' of its optimum value, it will appear to be very strong when compacted, but will tend to settle with time as the moisture content in the fill increases to equilibrium Cohesive soils such as the silty clay encountered may require high compaction energy to achieve acceptable densities if the moisture content is not close to their standard Proctor optimum value. It is therefore very important that the placement moisture content of the backfill soils be within 3 per cent of its standard Proctor optimum moisture content during placement and compaction.

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The backfilling and compaction operations should be monitored by a representative of SOIL-MAT to confirm uniform compaction of the backfill material to project specification requirements. We recommend that the lower layers of service trench backfill should be compacted to a minimum of 95 per cent of the material's standard Proctor maximum dry density [SPMDD], and the upper one metre of backfill compacted to 100 per cent of its SPMDD. The backfill should be placed in loose lifts not exceeding 300 millimetres, and should be compacted with the heaviest possible equipment that will not damage the pipe installation. The appropriate compaction equipment should be employed based on soil type, i.e. pad-toe for cohesive soils and smooth drum/vibratory plate for granular soils. Close supervision is prudent in areas that are not readily accessible to compaction equipment, for instance near the end of compaction 'runs', and around manholes. A method should be developed to assess compaction efficiency employing the on-site compaction equipment and backfill materials during construction

## 6. MANHOLES, CATCH BASINS AND THRUST BLOCKS

Properly prepared bearing surfaces for valve chambers, etc. in the native silty clay, stabilised where required, will be practically non-yielding under the anticipated loads. Proper preparation of the founding soils will tend to accentuate the protrusion of these structures above the pavement surface if compaction of the fill around these structures is not adequate, causing settlement of the surrounding paved surfaces. Conversely, the pavement surfaces may rise above the valve chambers and around manholes under frost action. To alleviate the potential for these types of differential movements, freedraining, non-frost susceptible material should be employed as backfill around the structures located within the paved roadway limits, and compacted to 100 per cent of its standard Proctor maximum dry density.

The thrust blocks in the native soils may be conservatively sized as recommended by the applicable Ontario Provincial Standard Specification conservatively using a horizontal allowable bearing pressure of up to 150 kPa [~3,000 psf]. Any backfill required behind the blocks should be a well-graded granular product and should be compacted to 100 per cent of its standard Proctor maximum dry density.

# 7. PAVEMENT RECONSTRUCTION CONSIDERATIONS

As noted above, the existing pavement structure was noted to consist of approximately 100 to 380 millimetres of asphaltic concrete overlying 300 to 600 millimetres of compacted granular base material. The pavement surface was noted to generally be in a relatively fair to poor condition, with some areas exhibiting frequent longitudinal,

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transverse, and alligator cracking, as well as repair patches. It is anticipated that the pavement structure will be simply saw cut along the limits of the excavation to allow for installation of the new sanitary system. In this regard, the contractor should exercise care along the saw cuts to prevent undermining of the granular base materials from beneath the asphaltic concrete, which would lead to future cracking of the asphalt. In the event that the asphaltic concrete surface becomes undermined, it will be necessary to extend the width of the saw cut portion beyond the undermined portion of the pavement. In such a case the pavement surface should be saw cut approximately 300 millimetres from the excavation edge. In the event that the excavation edge approaches the saw cut pavement edge closer than the 300 millimetre setback, it will be necessary

to reinstate the saw cut setback prior to repaving. It is anticipated that the pavement structure will be reinstated to 'match' the existing road surface, or be replaced with the applicable Haldimand County Standards. Alternatively, the recommended pavement

In the event that pavement reconstruction is to be completed as part of the sanitary replacement, based on the existing pavement structure and condition of the pavement surface, a partial depth reconstruction may be considered appropriate over the majority of the subject of roadway section, however, in areas of significant distress or where the existing pavement structure is considered deficient, a full depth reconstruction may be warranted. It is noted that a partial depth reconstruction would have a reduced lifespan and increased maintenance costs versus a full depth reconstruction.

#### PARTIAL DEPTH RECONSTRUCTION

structure as detailed below may be implemented.

Partial depth reconstruction of the pavement structure would typically consist of a 'peel and pave' method. This would involve the removal of the surficial asphalt, re-grading and compaction of the existing granular base material, and placement of new asphaltic concrete. It is recommended that after the existing asphalt layers have been removed the existing granular base material be re-compacted in place, and evaluated with a proof roll using a fully-loaded dump truck or large smooth drum roller in the presence of a representative of our office. Any areas of significant distress should be sub-excavated and replaced with quality granular material, compacted to 100 per cent of its standard Proctor maximum dry density [SPMDD].

The provision of good drainage will serve to improve the long-term performance of the pavement structure. Consideration should be given to the provision of new subdrains within the granular base material to promote drainage to existing catchbasins. Subdrains would typically consist of 100-millimetre diameter perforated plastic pipe encased in a geofabric sock. The sub-drains should be placed slightly below the subgrade level to promote good drainage.

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In terms of Granular Base Equivalence [GBE], it is noted that the total depth of the existing pavement structure over most of the study locations is generally equal to or greater than the pavement structure recommended below. As such, the placement of additional granular materials would generally be expected for levelling and grading purposes, or in areas of sub-excavation. The existing and any new granular base materials should be compacted to 100 per cent SPMDD. The recommended new asphaltic concrete pavement should consist of a minimum of 40 millimetres of HL3 surface course asphalt, over 80 millimetres of HL8 binder course asphalt. The new asphaltic concrete layers should be compacted to a minimum of 92 per cent of their Marshall maximum relative density [MRD]. Given the presence of existing concrete curbs and catchbasins, it is not anticipated that it will be feasible to raise the grade of the existing roadway, and as such a full depth reconstruction may be warranted if any areas

Given the depth of existing asphalt, a partial depth reconstruction consisting of a 'mill and pave' approach may also be considered. This approach would involve milling off the upper 40 to 50 millimetres of existing asphalt and replacing with a new lift of HL3 surface course material. It is noted that after milling the exposed surface should be reviewed for evidence of significant damage or distress that may warrant localised full removal and replacement of the asphalt layers. As well it may be prudent to consider the provision of a fibreglass mesh material to reinforce between the existing and new asphalt layers, which would assist in preventing reflection cracking. This is best assessed in the field at the time of the work.

are encountered with a reduced existing pavement structure.

#### FULL DEPTH RECONSTRUCTION

A full depth reconstruction of the pavement structure would provide for the best longterm performance of the new pavement. This approach would involve the removal of the existing asphaltic concrete layers and granular base materials to the proposed subgrade elevation. The existing asphaltic concrete could be pulverised into the existing granular base, and possibly mixed in with new imported granular fill material, to create a wellgraded granular product that could be re-used on the project as sub-base course material, depending on the material gradation. Laboratory sieve analyses would be required to assess the suitability of the pulverised/existing granular materials. The subgrade level would then be lowered to accommodate the required depths of the new pavement structure and finished grade.

The exposed subgrade should be proof rolled with 3 to 4 passes of a loaded tandem truck [over the same wheel path] in the presence of a representative of SOIL-MAT immediately prior to the placement of the sub-base material. Any areas of distress revealed by this or other means should be sub-excavated and replaced with suitable



backfill material, such as with suitable on-site granular materials or imported OPSS Granular 'B', Type II, compacted to 100 per cent of its SPMDD. Alternatively, the soft areas may be repaired by 'punching' coarse aggregate, such as a 50-millimetre clear crushed stone, into the soft areas. The need for sub-excavation of softened subgrade materials will be reduced if construction is undertaken during the dry summer months of the year and careful attention is paid to the compaction operations.

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Good drainage provisions will optimise the long-term performance of the pavement structure. The subgrade must be properly crowned and shaped to promote drainage to the subdrain system. Subdrains should be installed to intercept excess subsurface water and to prevent softening of the subgrade material. Surface water should not be allowed to pond adjacent to the outer limits of the paved areas.

The most severe loading conditions on the subgrade typically occur during the course of construction. Therefore, precautionary measures may have to be taken to ensure that the subgrade is not unduly disturbed by construction traffic.

The new pavement structure should satisfy the typical Haldimand County specifications. Alternatively, a recommended pavement structure to support cars, emergency vehicles, etc. for an arterial roadway would consist of a minimum of:

HL3 asphalt surface course	40 millimetres
HL8 asphalt binder course	80 millimetres
Base course granular [OPSS Granular 'A']	150 millimetres
Sub-base course granular [OPSS Granular 'B', Type II]	350 millimetres

It is our opinion, that this design is suitable for use on the subject roadway, provided that the subgrade has been prepared as detailed above before the sub-base course material is placed. If the subgrade is soft, remedial measures as discussed above may have to be implemented and/or the sub-base thickness may have to be increased. The granular sub-base and base courses should be compacted to 100 per cent of their SPMDD, and asphaltic concrete layers should be compacted to a minimum of 92 per cent of their Marshall maximum relative density [MRD]. A program of in-place density testing must be carried out to monitor that compaction requirements are being met.

The outlined full depth pavement reconstruction may be expected to have an approximate 20 to 25 year service life, assuming that regular maintenance is performed. Should a more detailed pavement structure design be required, site specific traffic information would be needed, together with detailed laboratory testing of the subgrade soils.

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## GENERAL ASPHALT PLACEMENT CONSIDERATIONS

To minimise segregation of the finished asphalt mat, the asphalt temperature must be maintained uniform throughout the mat during placement and compaction. All too often, significant temperature gradients exist in the delivered and placed asphalt with the cooler portions of the mat resisting compaction and presenting a honey combed surface. As the spreader moves forward, a responsible member of the paving crew should monitor the pavement surface, to ensure a smooth uniform surface. Surface segregation can be mitigated by 'back-casting' or scattering shovels of the full mix material over the segregated areas and raking out the coarse particles during compaction operations. Of course, the above assumes that the asphalt mix is sufficiently hot to allow the 'back-casting' to be performed.

## 9. ENVIRONMENTAL CONSIDERATIONS

As noted above, twenty one [21] selected samples of the subsurface soils recovered from the boreholes were submitted to an independent Canadian accredited analytical laboratory for background environmental testing for a standard panel of metal and inorganic parameters. The results of this testing are presented in the attached ALS Certificate of Analysis [L2120222].

The laboratory test results received in our Office were compared to the applicable standard from the <u>Soil, Ground Water and Sediment Standards</u> for Use under Part XV.1 of the *Environmental Protection Act*, as follows:

- TABLE 1: Full Depth Background Site Condition Standards for a Residential/ Parkland/ Institutional property use, [RPI], as well as for an Industrial/ Commercial/ Community [ICC] property use.
- TABLE 2: Full Depth Generic Site Condition Standards in a Potable Ground Water Condition for a Residential/Parkland/Institutional property use, [RPI], as well as for an Industrial/Commercial/Community [ICC] property use.
- TABLE 3: Full Depth Generic Site Condition Standards in a Non-Potable Ground Water Condition for a Residential/Parkland/Institutional property use, [RPI], as well as for an Industrial/Commercial/Community [ICC] property use.

Based on SOIL-MAT's field observations and the analytical test results from ALS, SOIL-MAT offers the following comments:



 All samples were found to meet the Table 1 [ALL] Standards for all parameters tested, with the exception of Chromium Hexavalent in Sample BH1 SS2, Cobalt in

Sample BH6 SS4, and Electrical Conductivity [EC] and/or Sodium Absorption Ratio [SAR] in all samples with the exception of Samples BH8 SS4 and BH8 SS5.

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2. All samples were found to meet the Table 2 and 3 [RPI] Standards for all parameters tested, with the exception of Electrical Conductivity [EC] and/or Sodium Absorption Ratio [SAR], which were found to exceed the standards in 17 of the 21 samples.

- 3. All samples were found to meet the Table 2 and 3 [ICC] Standards for all parameters tested, with the exception Electrical Conductivity [EC] and/or Sodium Absorption Ratio [SAR], which was found to exceed the standards in 11 of 21 samples.
- 4. It is noted that the presence of elevated levels of EC and SAR is often observed in the area of municipal roadways and parking lots and is largely the result of the use of salt for winter de-icing operations. EC and SAR are essentially aesthetic parameters that do not present a hazard to human or animal life. Rather they tend to render the soil environment un-supportive of plant growth and corrosive to buried grey or cast iron pipe;
- 5. The samples secured for analytical testing are believed to be representative of the soil conditions. No evidence of potential impact, i.e. staining or odours was observed during the fieldwork. If any significant changes are noted, i.e., odours, staining etc., SOIL-MAT should be contacted to reassess the environmental characteristics of the soil.

Given the above test results the following disposal options are applicable under Regulation 153/04 [amended by Regulation 511/09 effective July 1, 2011].

- As the tested material has been shown to exceed the Table 1 Standards, surplus material may not be accepted at an off-site Table 1 property, including property subject to a Record of Site Condition or MOE Certificate of Authorisation;
- As the test results for some of the submitted samples show values of EC and SAR which exceed the Table 2 and 3 RPI and ICC Standards, strictly speaking, the tested materials may not be accepted at an off-site RPI or ICC property in a potable or nonpotable groundwater condition.
- As the test results show only elevated levels of EC and/or SAR which exceed Table 2 and 3 RPI and ICC standards, noted above as essentially aesthetic parameters associated with the application of road de-icing salt, it would be reasonable to accept surplus material at an off-site RPI or ICC property under the 'beneficial use' concept. Such a use would require assessment of the receiving property and approval of the

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receiving property owner, and depending on the location and nature of the property consultation with the local MOE District Engineer;

Excavated soil may be reused as backfill on site.

## 10. GENERAL COMMENTS

The comments provided in this document are intended only for the guidance of the design team. The subsoil descriptions and borehole information are intended to describe conditions at the borehole locations. Contractors tendering or undertaking this project should carry out due diligence in order to verify the results of this investigation and to determine how the subsurface conditions will affect their operations.

We trust that this geotechnical report is sufficient for your present requirements. Should you require any additional information or clarification as to the contents of this document, please do not hesitate to contact the undersigned.

Yours very truly,

SOIL-MAT ENGINEERS & CONSULTANTS LTD.

Adam Roemmele, B.Eng., EIT

Kyle Richardson, P.Eng. Project Engineer

Matt LiVecchi, P. Eng.

Project Engineer

Enclosures:

Drawing No. 1 to 2, Borehole Location Plans

NCE OF O

Log of Borehole Nos. 1 through 10
ALS Certificates of Analysis [L2120222]

Distribution: Haldimand County [3, plus pdf]



#### **LEGEND**



**Borehole Location** 

#### NOTES

- 1. This drawing should be read in conjunction with Soil-Mat Engineers & Consultants Ltd. Report No. SM 188337-G.
- 2. Borehole locations are approximate.

# SOIL-MAT

ENGINEERS & CONSULTANTS LTD.

Geotechnical Investigation Proposed Intersection Improvements, Argyle Street Caledonia, Ontario

**Borehole Location Plan** 

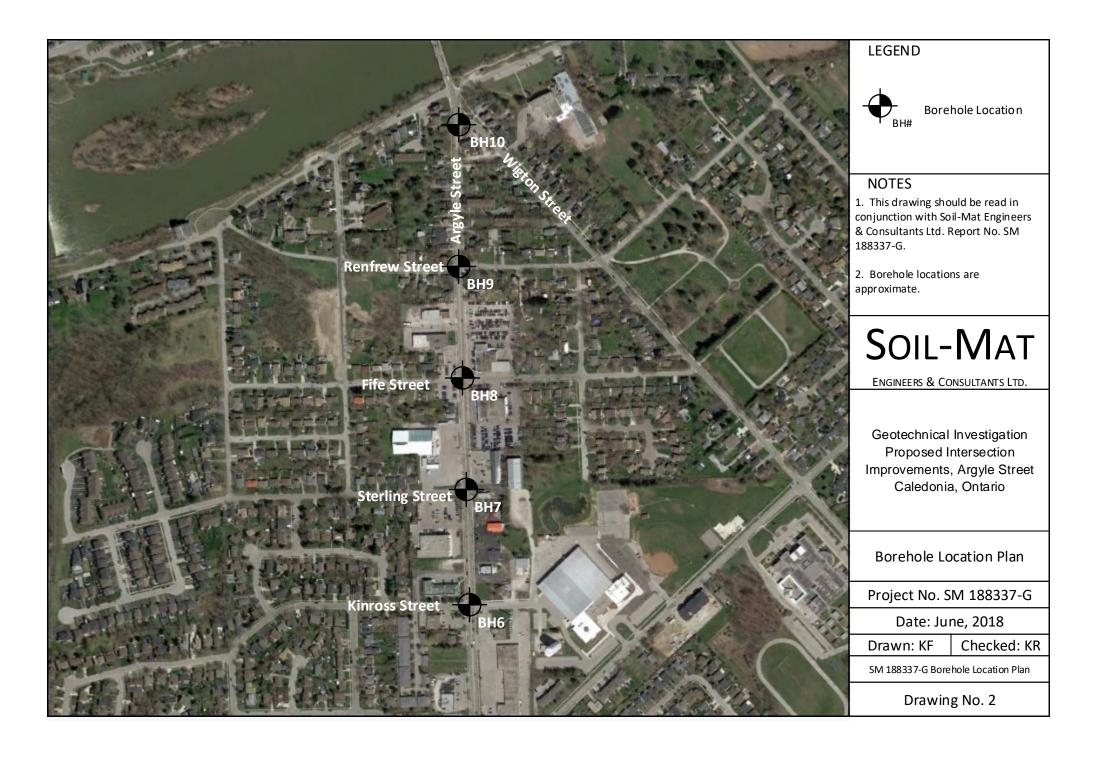
Project No. SM 188337-G

Date: June, 2018

Drawn: KF Checked: KR

SM 188337-G Borehole Location Plan

Drawing No. 1



Project No: SM 188337-GProject Manager: Kyle Richardson, P.Eng.Project: Proposed Intersection ImprovementsBorehole Location: See Drawing No.1

Location: Argyle Street and Haddington Street : Client: Haldimand County - Engineering Division :



							SAMI	PLE				Moisture Content
Depth	Elevation (m)	Symbol	Description	Well Data	Туре	Number	Blow Counts	Blows/300mm	Recovery	PP (kgf/cm2)	U.Wt.(kN/m3)	\$\text{w\\\ 10 \ 20 \ 30 \ 40}\$\$\$  Standard Penetration Test  blows/300mm  20 \ 40 \ 60 \ 80\$\$
ft m			Ground Surface		·		_		_	_		
1	-0.30		Sand and Gravel Fill Approximately 300 millimetres of		SS	1	18 20 8	28				*
2  3   .	-0.91	1	crushed limestone aggregate.  Silty Clay		SS	2	687	15		>4.5		
ft m 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 17 24 25 18 19 20 17 24 25 18 19 20 21 22 23 24 25 25 25 25 25 25 25 25 25 25 25 25 25		1	Brown, trace sand and gravel, reworked in upper levels, stiff to very stiff.									
6 2			End of Borehole									
8												
9 3												
11 12												
13 4												
14 <u>1</u>												
16 5												
18												
19 20 6												
21												
23 7												
24 <del>*</del> 25 <b>*</b>			NOTES:									
26 8 27 8			Borehole was advanced using solid stem auger equipment on June 22, 2018 to termination at a depth of 0.9 metres.									
26 27 28 29 30 31 31 31 31 31 31 31 31 31 31 31 31 31			Borehole was recorded as 'dry' upon completion of drilling and backfilled as per Ontario Regulation 903.									
32 🛊			Soil samples will be discarded after 3 months unless otherwise directed by our client.									
33								<u> </u>				

**Drill Method:** Solid Stem Augers **Drill Date:** June 22, 2018

Hole Size: 150 Millimetres

Drilling Contractor: Elite Drilling

Soil-Mat Engineers & Consultants Ltd.

130 Lancing Drive, Hamilton, ON L8W 3A1 T: 905.318.7440 F: 905.318.7455

E: info@soil-mat.ca

**Datum:** Existing Road Surface

Field Logged by: KF Checked by: KR

Project No: SM 188337-GProject Manager: Kyle Richardson, P.Eng.Project: Proposed Intersection ImprovementsBorehole Location: See Drawing No.1

Location: Argyle Street South

Client: Haldimand County - Engineering Division:



							SAMI	PLE					isture Con	itent
Depth	Elevation (m)	Symbol	Description	Well Data	ē	Number	Blow Counts	Blows/300mm	Recovery	PP (kgf/cm2)	U.Wt.(kN/m3)		w% 20 30 rd Penetra lows/300m	
ft m		Syr		We	Туре	Nur	Blo	B	Rec	윤	). ).	20	40 60	
0 m m	0.00		Ground Surface Pavement Structure											
2 3	-0.78		Approximately 380 millimetres of											
4 1			Silty Clay Brown to greyish brown, trace sand and gravel, trace organics and		SS	1	4 4 4 5	8		<1				
6 2			reworked in upper levels, firm to stiff.		SS	2	4577	12		3.0		<b>,</b>		
8					ss	3	3 4 4 4	8		<1		<b> </b>		
10 3					ss	4	3 4 5	9		<1				
11 1	-3.51	11.	End of Borehole		33	4	343	9					_	
th     1     2     3     4     5     6     7     8     9     10     11     12     13     14     15     16     17     18     19     20     21     22     22     26     27     28     29     30     31     32     33       3     3     3     3     3     3     33     33     33			NOTES:  1. Borehole was advanced using solid stem auger equipment on June 22, 2018 to termination at a depth of 3.5 metres.  2. Borehole was recorded as 'dry' upon completion of drilling and backfilled as per Ontario Regulation 903.  3. Soil samples will be discarded after 3 months unless otherwise directed by our client.											

**Drill Method:** Solid Stem Augers

Drill Date: June 22, 2018Hole Size: 150 MillimetresDrilling Contractor: Elite Drilling

Soil-Mat Engineers & Consultants Ltd.

130 Lancing Drive, Hamilton, ON L8W 3A1

T: 905.318.7440 F: 905.318.7455

E: info@soil-mat.ca

**Datum:** Existing Road Surface

Field Logged by: KF Checked by: KR

Project No: SM 188337-GProject Manager: Kyle Richardson, P.Eng.Project: Proposed Intersection ImprovementsBorehole Location: See Drawing No.1

Location: Argyle Street and Haddington Street : Client: Haldimand County - Engineering Division :



							SAMI	PLE				Moisture Content
Depth	Elevation (m)	Symbol	Description	Well Data	Туре	Number	Blow Counts	Blows/300mm	Recovery	PP (kgf/cm2)	U.Wt.(kN/m3)	\$\begin{array}{c ccccc} \ & & & & & & & & & & & & & & & & & &
ft m	0.00		Ground Surface									
	-0.30	7~	Topsoil Approximately 300 millimetres of topsoil.		SS	1	3765	13				
3 1	-1.22		Silty Clay  Brown, trace sand and gravel, trace  organics and reworked in upper levels,		SS	2	235	8		2.5		\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \
5			firm to stiff.  End of Borehole									
Text     Text   Text   Text     Text			NOTES:  1. Borehole was advanced using solid stem auger equipment on June 22, 2018 to termination at a depth of 1.2 metres.  2. Borehole was recorded as 'dry' upon completion of drilling and backfilled as per Ontario Regulation 903.  3. Soil samples will be discarded after 3 months unless otherwise directed by our client.									

**Drill Method:** Solid Stem Augers

Drill Date: June 22, 2018Hole Size: 150 MillimetresDrilling Contractor: Elite Drilling

Soil-Mat Engineers & Consultants Ltd.

130 Lancing Drive, Hamilton, ON L8W 3A1 T: 905.318.7440 F: 905.318.7455

E: info@soil-mat.ca

**Datum:** Existing Road Surface

Field Logged by: KF Checked by: KR

Project No: SM 188337-GProject Manager: Kyle Richardson, P.Eng.Project: Proposed Intersection ImprovementsBorehole Location: See Drawing No.1

Location: Haddington Street

Client: Haldimand County - Engineering Division:



							SAMF	PLE				Moisture Content
Depth	Elevation (m)	Symbol	Description	Well Data	Туре	Number	Blow Counts	Blows/300mm	Recovery	PP (kgf/cm2)	U.Wt.(kN/m3)	10 20 30 40  Standard Penetration Test  ■ blows/300mm  20 40 60 80
ft m	0.00	444	Ground Surface									
1 2 2	-0.70		Pavement Structure Approximately 100 millimetres of asphatic concrete over 600 millimetres of compact granular base.		SS	1	18 16 13 7	29				
3 1			Silty Clay Brown to greyish brown, trace sand		SS	2	4557	10		2.5		
6 2			and gravel, reworked in upper levels, firm to stiff.		SS	3	3346	7		2.5		
8 9 9					SS	4	3356	8		2.5		<b> </b>
10 3	-3.66	###	End of Borehole		SS	5	2355	8		2.0		
ft     m 0       1     2       3     4       4     5       6     7       8     9       10     12       13     14       15     16       17     18       19     20       22     23       23     24       24     25       26     27       28     29       30     31       31     32       33     33			NOTES:  1. Borehole was advanced using solid stem auger equipment on June 22, 2018 to termination at a depth of 3.7 metres.  2. Borehole was recorded as 'dry' upon completion of drilling and backfilled as per Ontario Regulation 903.  3. Soil samples will be discarded after 3 months unless otherwise directed by our client.									

**Drill Method:** Solid Stem Augers **Drill Date:** June 22, 2018

Hole Size: 150 Millimetres

Drilling Contractor: Elite Drilling

Soil-Mat Engineers & Consultants Ltd.

130 Lancing Drive, Hamilton, ON L8W 3A1 T: 905.318.7440 F: 905.318.7455

E: info@soil-mat.ca

**Datum:** Existing Road Surface

Field Logged by: KF Checked by: KR

Project No: SM 188337-GProject Manager: Kyle Richardson, P.Eng.Project: Proposed Intersection ImprovementsBorehole Location: See Drawing No.1

Location: Argyle Street South

Client: Haldimand County - Engineering Division :



							SAMI	PLE				Moisture Content
Depth	Elevation (m)	Symbol	Description	Well Data	Туре	Number	Blow Counts	Blows/300mm	Recovery	PP (kgf/cm2)	U.Wt.(kN/m3)	\$\text{N} \chi_w\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\
$\int_{0}^{\infty} \int_{0}^{\infty} dt$	0.00	444	Ground Surface									
1 2 2	-0.70		Pavement Structure Approximately 100 millimetres of asphatic concrete over 600 millimetres of compact granular base.		SS	1	22 12 7 6	19				
3 1 4 1			Silty Clay Brown to greyish brown, trace sand		ss	2	4546	9		3.5		
6 2			and gravel, reworked in upper levels, firm to stiff.		SS	3	4478	11		3.5		
8 9 9					SS	4	3356	8		3.0		
10 3	-3.66				SS	5	2457	9		2.0		
ft			NOTES:  1. Borehole was advanced using solid stem auger equipment on June 22, 2018 to termination at a depth of 3.7 metres.  2. Borehole was recorded as 'dry' upon completion of drilling and backfilled as per Ontario Regulation 903.  3. Soil samples will be discarded after 3 months unless otherwise directed by our client.									

**Drill Method:** Solid Stem Augers

Drill Date: June 22, 2018

Hole Size: 150 Millimetres

Drilling Contractor: Elite Drilling

Soil-Mat Engineers & Consultants Ltd.

130 Lancing Drive, Hamilton, ON L8W 3A1

T: 905.318.7440 F: 905.318.7455 E: info@soil-mat.ca

**Datum:** Existing Road Surface

Field Logged by: KF Checked by: KR Sheet: 1 of 1

Project No: SM 188337-GProject Manager: Kyle Richardson, P.Eng.Project: Proposed Intersection ImprovementsBorehole Location: See Drawing No.1

Location: Argyle Street South

Client: Haldimand County - Engineering Division :



							SAMF	PLE				Moisture Content
Depth	Elevation (m)	Symbol	Description	Well Data	Туре	Number	Blow Counts	Blows/300mm	Recovery	PP (kgf/cm2)	U.Wt.(kN/m3)	\$\text{N} \text{W} \text{\frac{1}{0}} \text{20} \text{30} \text{40}\$\$  Standard Penetration Test blows/300mm \text{\frac{1}{0}} \text{20} \text{40} \text{60} \text{80}\$\$
ft m	0.00		Ground Surface									
1 2	-0.80		Pavement Structure Approximately 200 millimetres of asphatic concrete over 600 millimetres		ss	1	11 21 19 17	40				
3 1 4 1 5 1		###	of compact granular base.  Silty Clay  Brown to greyish brown, trace sand and gravel, reworked in upper levels,		SS	2	10 6 5 7	11		3.0		
6 2			firm to stiff.		SS	3	4589	13		3.5		
9 3												
11 12					SS	4	2357	8		2.5		<b> </b>
13 4		# #										
16 16 17	-5.18	###			SS	5	2355	8		2.0		
ft       0       1       2       3       4       5       6       7       8       9       10       11       13       14       15       16       17       18       19       20       21       22       23       24       25			End of Borehole									
22 23 7 24			NOTES:									
25 8 26 8			Borehole was advanced using solid stem auger equipment on June 22, 2018 to termination at a depth of 5.2 metres.									
28 29 30 30			Borehole was recorded as 'dry' upon completion of drilling and backfilled as per Ontario Regulation 903.									
26 27 28 29 30 31 32 33 33 33			Soil samples will be discarded after 3 months unless otherwise directed by our client.									
<u>ეა                                    </u>												

**Drill Method:** Solid Stem Augers

Drill Date: June 22, 2018Hole Size: 150 MillimetresDrilling Contractor: Elite Drilling

Soil-Mat Engineers & Consultants Ltd.

130 Lancing Drive, Hamilton, ON L8W 3A1

T: 905.318.7440 F: 905.318.7455

E: info@soil-mat.ca

**Datum:** Existing Road Surface

Field Logged by: KF Checked by: KR

Project No: SM 188337-GProject Manager: Kyle Richardson, P.Eng.Project: Proposed Intersection ImprovementsBorehole Location: See Drawing No.1

Location: Argyle Street South

Client: Haldimand County - Engineering Division:



							SAMF	PLE				Moisture Content
Depth	Elevation (m)	Symbol	Description	Well Data	Туре	Number	Blow Counts	Blows/300mm	Recovery	PP (kgf/cm2)	U.Wt.(kN/m3)	\$\text{N} \chi_w\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\
$\frac{\text{ft m}}{0 = 0}$	0.00		Ground Surface									
1 2 2	-0.90		Pavement Structure Approximately 300 millimetres of asphatic concrete over 600 millimetres of compact granular base.		SS	1	48 31 30 17	61				
3 <del> </del> 1   4     1		###	Silty Clay Brown to greyish brown, trace sand		SS	2	10 5 7 7	12		3.5		
6 2			and gravel, reworked in upper levels, stiff to firm.		ss	3	1232	5		1.5		
9 3		###										
11 12					ss	4	1345	7		1.5		
13 4												
16 5 17 5	-4.88 -5.18		Transition to grey in colour		SS	5	2334	6		<1		
ft			End of Borehole									
24 🕌			NOTES:									
25 8 26 8 27			Borehole was advanced using solid stem auger equipment on June 22, 2018 to termination at a depth of 5.2 metres.									
26 27 28 29 30 31 32 33 33			Borehole was recorded as 'dry' upon completion of drilling and backfilled as per Ontario Regulation 903.									
31 32 33			<ol> <li>Soil samples will be discarded after 3 months unless otherwise directed by our client.</li> </ol>									
32												

**Drill Method:** Solid Stem Augers

Drill Date: June 22, 2018Hole Size: 150 MillimetresDrilling Contractor: Elite Drilling

Soil-Mat Engineers & Consultants Ltd.

130 Lancing Drive, Hamilton, ON L8W 3A1

T: 905.318.7440 F: 905.318.7455

E: info@soil-mat.ca

**Datum:** Existing Road Surface

Field Logged by: KF Checked by: KR

Project No: SM 188337-GProject Manager: Kyle Richardson, P.Eng.Project: Proposed Intersection ImprovementsBorehole Location: See Drawing No.1

Location: Argyle Street South

Client: Haldimand County - Engineering Division :



							SAMF	PLE				Moisture Content
Depth	Elevation (m)	Symbol	Description	Well Data	Туре	Number	Blow Counts	Blows/300mm	Recovery	PP (kgf/cm2)	U.Wt.(kN/m3)	\$w\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\
ft m	0.00		Ground Surface									
1 2	-0.80		Pavement Structure Approximately 200 millimetres of asphatic concrete over 600 millimetres of compact granular base.		SS	1	6 13 16 8	29				
3 1		# #	Silty Clay Brown to greyish brown, trace sand		ss	2	6 4 5 4	9		<1		
6 2		###	and gravel, reworked in upper levels, stiff to firm.		SS	3	2346	7		2.5		
T												
11	-3.35		Transition to grey in colour.		SS	4	2244	6		<1		
13 4		<del>+</del>										
16 5 17 5					ss	5	2235	5		<1		
18		H H										
20 + 21 + 22 + 22 + 22 + 22 + 22 + 22 +	-6.71	H H			ss	6	2233	5		<1		
23 7 24			End of Borehole  NOTES:									
25 8 26 8			Borehole was advanced using solid stem auger equipment on June 22, 2018 to termination at a depth of 6.7 metres.									
28 29 9			Borehole was recorded as 'dry' upon completion of drilling and backfilled as per Ontario Regulation 903.									
26 27 28 29 30 31 32 33 33 33			Soil samples will be discarded after 3 months unless otherwise directed by our client.									
-	1									<u> </u>		

**Drill Method:** Solid Stem Augers **Drill Date:** June 22, 2018

Hole Size: 150 Millimetres

Drilling Contractor: Elite Drilling

Soil-Mat Engineers & Consultants Ltd.

130 Lancing Drive, Hamilton, ON L8W 3A1 T: 905.318.7440 F: 905.318.7455

E: info@soil-mat.ca

**Datum:** Existing Road Surface

Field Logged by: KF Checked by: KR

Project No: SM 188337-GProject Manager: Kyle Richardson, P.Eng.Project: Proposed Intersection ImprovementsBorehole Location: See Drawing No.1

Location: Argyle Street South

Client: Haldimand County - Engineering Division :



							SAMF	PLE				Moisture Content
Depth	Elevation (m)	Symbol	Description	Well Data	Туре	Number	Blow Counts	Blows/300mm	Recovery	PP (kgf/cm2)	U.Wt.(kN/m3)	\$\text{N} \text{\chi_w\%} \text{\chi} \tex
ft m	0.00		Ground Surface									
	-0.90		Pavement Structure Approximately 300 millimetres of asphatic concrete over 600 millimetres of compact granular base.		SS	1	40 38 23 12	61				
3 1	0.00	T T	Silty Clay Brown to greyish brown, trace sand		ss	2	6345	7		3.0		
6 2		#	and gravel, reworked in upper levels, stiff to firm.		ss	3	4478	11		3.5		
The state of the												
11 12					SS	4	4456	9		4.0		
13 4 14	-4.10		Transition to grey in colour.									
15 16 5		H H			ss	5	1322	5		<1		<b> </b>
13 14 14 15 16 17 18 19 19 19 19 19 19 19 19 19 19 19 19 19												
20 6	-6.71				SS	6	2232	5		<1		
23 7 24 7			End of Borehole  NOTES:									
25 8 26 8			Borehole was advanced using solid stem auger equipment on June 22, 2018 to termination at a depth of 6.7 metres.									
26 27 28 29 30 31 32 33 33			Borehole was recorded as 'dry' upon completion of drilling and backfilled as per Ontario Regulation 903.									
31 32			Soil samples will be discarded after 3 months unless otherwise directed by our client.									
33-											<u> </u>	

**Drill Method:** Solid Stem Augers

Drill Date: June 22, 2018

Hole Size: 150 Millimetres

Drilling Contractor: Elite Drilling

Soil-Mat Engineers & Consultants Ltd.

130 Lancing Drive, Hamilton, ON L8W 3A1

T: 905.318.7440 F: 905.318.7455

E: info@soil-mat.ca

**Datum:** Existing Road Surface

Field Logged by: KF Checked by: KR

Project No: SM 188337-GProject Manager: Kyle Richardson, P.Eng.Project: Proposed Intersection ImprovementsBorehole Location: See Drawing No.1

Location: Argyle Street South

Client: Haldimand County - Engineering Division:



								SAMF	PLE				Moisture Content
Depth		Elevation (m)	Symbol	Description	Well Data	Туре	Number	Blow Counts	Blows/300mm	Recovery	PP (kgf/cm2)	U.Wt.(kN/m3)	No.   No.
ft r	n <sub>0</sub> 0.	.00		Ground Surface									
1 2 1	-0	0.80		Pavement Structure Approximately 200 millimetres of asphatic concrete over 600 millimetres of compact granular base.		SS	1	11 19 13 14	32				
4 4 5	1		: :	Sand and Gravel Fill Brown, compact.		ss	2	13 12 10 12	22				
6	2 -2	2.10				ss	3	10 10 15 10	25				
8 9 10	- 3			Silty Clay Brown to greyish brown, trace sand and gravel, reworked in upper levels, stiff to hard.		SS	4	6 8 11 12	19		3.5		
11 12 12						SS	5	3467	10		3.5		
13 14 15	4												
16 17	55	5.18				SS	6	4 14 18 19	32		>4.5		
18	6			End of Borehole									
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25	7												
24				NOTES:									
25 26 27	8			Borehole was advanced using solid stem auger equipment on June 22, 2018 to termination at a depth of 5.2 metres.									
26 24 29 30 31 32 31 32 31 32 31 32 31 32 31 32 31 32 31 32 31 32 31 32 31 31 32 31 31 31 31 31 31 31 31 31 31 31 31 31	9			Borehole was recorded as 'dry' upon completion of drilling and backfilled as per Ontario Regulation 903.									
31 32 33				Soil samples will be discarded after 3 months unless otherwise directed by our client.									

**Drill Method:** Solid Stem Augers

Drill Date: June 22, 2018Hole Size: 150 MillimetresDrilling Contractor: Elite Drilling

Soil-Mat Engineers & Consultants Ltd.

130 Lancing Drive, Hamilton, ON L8W 3A1 T: 905.318.7440 F: 905.318.7455

E: info@soil-mat.ca

**Datum:** Existing Road Surface

Field Logged by: KF Checked by: KR



Soil Mat Engineers & Consulting Ltd.

(Hamilton)

ATTN: Kyle Richardson

130 Lancing Drive

Hamilton ON L8W 3A1

Date Received: 27-JUN-18

Report Date: 05-JUL-18 14:28 (MT)

Version: FINAL

Client Phone: 905-318-7440

# Certificate of Analysis

Lab Work Order #: L2120222

Project P.O. #: NOT SUBMITTED

Job Reference: 188337

C of C Numbers: Legal Site Desc:

Mary-Lynn Pike Client Services Supervisor

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L2120222 CONT'D....

Job Reference: 188337

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05-JUL-18 14:28 (MT)

# **Summary of Guideline Exceedances**

Suideline ALS ID	Client ID	Grouping	Analyte	Result	Guideline Limit	Unit
ntario Reg	gulation 153/04 - April 15	5, 2011 Standards - T1-Soil-Res/Park/Iı	nst/Ind/Com/Commu Property Use			
.2120222-1	BH1 SS2	Physical Tests	Conductivity	0.619	0.57	mS/cm
		Speciated Metals	Chromium, Hexavalent	1.01	0.66	ug/g
2120222-2	BH3 SS2	Physical Tests	Conductivity	0.913	0.57	mS/cm
		Saturated Paste Extractables	SAR	11.9	2.4	SAR
2120222-3	BH2 SS1	Physical Tests	Conductivity	5.61	0.57	mS/cm
		Saturated Paste Extractables	SAR	12.0	2.4	SAR
2120222-4	BH2 SS2	Physical Tests	Conductivity	1.32	0.57	mS/cm
2120222-5	BH2 SS3	Physical Tests	Conductivity	1.01	0.57	mS/cm
2120222-6	BH4 SS2	Physical Tests	Conductivity	2.24	0.57	mS/cm
		Saturated Paste Extractables	SAR	30.0	2.4	SAR
2120222-7	BH4 SS3	Physical Tests	Conductivity	1.50	0.57	mS/cm
		Saturated Paste Extractables	SAR	8.74	2.4	SAR
120222-8	BH4 SS4	Physical Tests	Conductivity	0.640	0.57	mS/cm
120222-9	BH5 SS2	Physical Tests	Conductivity	0.879	0.57	mS/cm
		Saturated Paste Extractables	SAR	13.5	2.4	SAR
2120222-10	BH5 SS3	Physical Tests	Conductivity	0.761	0.57	mS/cm
		Saturated Paste Extractables	SAR	10.3	2.4	SAR
2120222-11	BH5 SS4	Physical Tests	Conductivity	0.907	0.57	mS/cm
		Saturated Paste Extractables	SAR	8.78	2.4	SAR
2120222-12	BH6 SS2	Physical Tests	Conductivity	8.18	0.57	mS/cm
		Saturated Paste Extractables	SAR	34.8	2.4	SAR
2120222-13	BH6 SS3	Physical Tests	Conductivity	7.08	0.57	mS/cm
		Saturated Paste Extractables	SAR	17.0	2.4	SAR
2120222-14	BH6 SS4	Physical Tests	Conductivity	0.913	0.57	mS/cm
		Saturated Paste Extractables	SAR	3.90	2.4	SAR
		Metals	Cobalt (Co)	21.3	21	ug/g
120222-15	BH8 SS2	Physical Tests	Conductivity	10.7	0.57	mS/cm
		Saturated Paste Extractables	SAR	31.2	2.4	SAR
120222-16	BH8 SS3	Physical Tests	Conductivity	6.73	0.57	mS/cm
		Saturated Paste Extractables	SAR	20.3	2.4	SAR
2120222-19	BH10 SS2	Physical Tests	Conductivity	5.86	0.57	mS/cm

<sup>\*</sup> Please refer to the Reference Information section for an explanation of any qualifiers noted.



L2120222 CONT'D....

Job Reference: 188337

PAGE 3 of 20

05-JUL-18 14:28 (MT)

# **Summary of Guideline Exceedances**

Guideline ALS ID	Client ID	Grouping	Analyte	Result	Guideline Limit	Unit
Ontario Reg	julation 153/04	- April 15, 2011 Standards - T1-Soil-Res/Park/In	st/Ind/Com/Commu Property Use			
L2120222-19	BH10 SS2	Saturated Paste Extractables	SAR	17.4	2.4	SAR
L2120222-20	BH10 SS3	Physical Tests	Conductivity	2.67	0.57	mS/cm
		Saturated Paste Extractables	SAR	7.40	2.4	SAR
L2120222-21	BH10 SS5	Physical Tests Saturated Paste Extractables	Conductivity SAR	5.05 9.46	0.57 2.4	mS/cm SAR

<sup>\*</sup> Please refer to the Reference Information section for an explanation of any qualifiers noted.



L2120222 CONT'D....

Job Reference: 188337

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05-JUL-18 14:28 (MT)

**Physical Tests - SOIL** 

i ilyaicai reala - aoil											
		Lab	<b>D</b> L2120222-1	L2120222-2	L2120222-3	L2120222-4	L2120222-5	L2120222-6	L2120222-7	L2120222-8	L2120222-9
	;	Sample Da	te 22-JUN-18	22-JUN-18	22-JUN-18	22-JUN-18	22-JUN-18	22-JUN-18	22-JUN-18	22-JUN-18	22-JUN-18
		Sample	ID BH1 SS2	BH3 SS2	BH2 SS1	BH2 SS2	BH2 SS3	BH4 SS2	BH4 SS3	BH4 SS4	BH5 SS2
Analyte	Unit	Guide Lim #1 #2									
Conductivity	mS/cm	0.57 -	0.619	0.913	5.61	1.32	1.01	2.24	1.50	0.640	0.879
% Moisture	%		18.0	22.0	18.5	16.1	20.3	16.2	24.1	25.0	19.1
pH	pH units		7.36	7.43	6.90	7.46	7.45	7.75	7.73	7.66	7.28

Guide Limit #1: T1-Soil-Res/Park/Inst/Ind/Com/Commu Property Use

<sup>\*</sup> Please refer to the Reference Information section for an explanation of any qualifiers noted.



L2120222 CONT'D....

Job Reference: 188337

PAGE 5 of 20

05-JUL-18 14:28 (MT)

**Physical Tests - SOIL** 

i ilyalodi i cata dole											
		Lab	<b>ID</b> L2120222-10	L2120222-11	L2120222-12	L2120222-13	L2120222-14	L2120222-15	L2120222-16	L2120222-17	L2120222-18
	,	Sample Da	te 22-JUN-18	22-JUN-18	22-JUN-18	22-JUN-18	22-JUN-18	22-JUN-18	22-JUN-18	22-JUN-18	22-JUN-18
		Sample	ID BH5 SS3	BH5 SS4	BH6 SS2	BH6 SS3	BH6 SS4	BH8 SS2	BH8 SS3	BH8 SS4	BH8 SS5
Analyte	Unit	Guide Lim #1 #2									
Conductivity	mS/cm	0.57 -	0.761	0.907	8.18	7.08	0.913	10.7	6.73	0.533	0.195
% Moisture	%		9.57	18.3	15.8	17.6	23.0	20.9	21.0	25.2	21.3
pH	pH units		7.65	7.54	7.83	7.64	7.61	7.62	7.68	7.75	7.76

Guide Limit #1: T1-Soil-Res/Park/Inst/Ind/Com/Commu Property Use

<sup>\*</sup> Please refer to the Reference Information section for an explanation of any qualifiers noted.



L2120222 CONT'D....

Job Reference: 188337

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**Physical Tests - SOIL** 

i ilyolodi i coto COIL						
		L	_ab ID	L2120222-19	L2120222-20	L2120222-21
	5	Sample	e Date	22-JUN-18	22-JUN-18	22-JUN-18
		Sam	ple ID	BH10 SS2	BH10 SS3	BH10 SS5
Analyte	Unit	Guide #1	Limits #2			
Conductivity	mS/cm	0.57	-	5.86	2.67	5.05
% Moisture	%	-	-	8.54	5.93	25.6
pH	pH units	-	-	8.00	7.93	7.63

Guide Limit #1: T1-Soil-Res/Park/Inst/Ind/Com/Commu Property Use

<sup>\*</sup> Please refer to the Reference Information section for an explanation of any qualifiers noted.



L2120222 CONT'D....

Job Reference: 188337

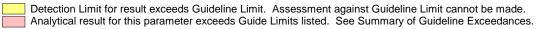
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Cyanides - SOIL

- January												
		La	ab ID	L2120222-1	L2120222-2	L2120222-3	L2120222-4	L2120222-5	L2120222-6	L2120222-7	L2120222-8	L2120222-9
		Sample	Date	22-JUN-18								
		Samp	ole ID	BH1 SS2	BH3 SS2	BH2 SS1	BH2 SS2	BH2 SS3	BH4 SS2	BH4 SS3	BH4 SS4	BH5 SS2
		Guide L	imits									
Analyte	Unit		#2									
Cyanide, Weak Acid Diss		0.051		<0.050	<0.050	<0.050	< 0.050	<0.050	<0.050	<0.050	<0.050	<0.050

Guide Limit #1: T1-Soil-Res/Park/Inst/Ind/Com/Commu Property Use



<sup>\*</sup> Please refer to the Reference Information section for an explanation of any qualifiers noted.



L2120222 CONT'D....

Job Reference: 188337

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Cyanides - SOIL

Analyte	Unit		#2									
		Guide Li	mite									
		Sampl	e ID	BH5 SS3	BH5 SS4	BH6 SS2	BH6 SS3	BH6 SS4	BH8 SS2	BH8 SS3	BH8 SS4	BH8 SS5
		Sample I	Date	22-JUN-18								
		La	b ID	L2120222-10	L2120222-11	L2120222-12	L2120222-13	L2120222-14	L2120222-15	L2120222-16	L2120222-17	L2120222-18

Guide Limit #1: T1-Soil-Res/Park/Inst/Ind/Com/Commu Property Use

<sup>\*</sup> Please refer to the Reference Information section for an explanation of any qualifiers noted.



L2120222 CONT'D....

Job Reference: 188337

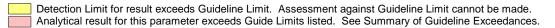
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## **Cyanides - SOIL**

Cyanide, Weak Acid Diss	ug/g	0.051	-	<0.050	<0.050	<0.050
Analyte	Unit	Guide #1	Limits #2			
		Sam	ple ID	BH10 SS2	BH10 SS3	BH10 SS5
		Sample	Date	22-JUN-18	22-JUN-18	22-JUN-18
		L	.ab ID	L2120222-19	L2120222-20	L2120222-21

#### Guide Limit #1: T1-Soil-Res/Park/Inst/Ind/Com/Commu Property Use



<sup>\*</sup> Please refer to the Reference Information section for an explanation of any qualifiers noted.



L2120222 CONT'D....

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#### Saturated Paste Extractables - SOIL

Oaturated raste Extractables	OOIL											
		l	Lab ID	L2120222-1	L2120222-2	L2120222-3	L2120222-4	L2120222-5	L2120222-6	L2120222-7	L2120222-8	L2120222-9
		Sample	e Date	22-JUN-18								
		Sam	ple ID	BH1 SS2	BH3 SS2	BH2 SS1	BH2 SS2	BH2 SS3	BH4 SS2	BH4 SS3	BH4 SS4	BH5 SS2
		Guide	Limits									
Analyte	Unit	#1	#2									
SAR	SAR	2.4	-	0.99	11.9	12.0	1.41	2.05	30.0	8.74	1.08	13.5 SAR:M
Calcium (Ca)	mg/L	-	-	50.9	12.6	239	138	89.3	11.3	38.0	23.9	10.5
Magnesium (Mg)	mg/L	-	-	8.1	1.3	37.2	7.3	3.6	2.6	7.7	25.8	<1.0
Sodium (Na)	mg/L	-	-	28.9	166	757	62.8	72.5	430	226	32.0	159

Guide Limit #1: T1-Soil-Res/Park/Inst/Ind/Com/Commu Property Use

<sup>\*</sup> Please refer to the Reference Information section for an explanation of any qualifiers noted.



L2120222 CONT'D....

Job Reference: 188337

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#### Saturated Paste Extractables - SOIL

Catarated I aste Extractables	OOIL											
		ı	Lab ID	L2120222-10	L2120222-11	L2120222-12	L2120222-13	L2120222-14	L2120222-15	L2120222-16	L2120222-17	L2120222-18
		Sample	e Date	22-JUN-18								
		Sam	ple ID	BH5 SS3	BH5 SS4	BH6 SS2	BH6 SS3	BH6 SS4	BH8 SS2	BH8 SS3	BH8 SS4	BH8 SS5
		Guide	Limits									
Analyte	Unit	#1	#2									
SAR	SAR	2.4	-	10.3 SAR:M	8.78	34.8	17.0	3.90	31.2	20.3	0.39	0.40
Calcium (Ca)	mg/L	-	-	11.5	16.9	92.8	251	43.3	196	163	36.1	9.0
Magnesium (Mg)	mg/L	-	-	<1.0	2.4	11.4	19.5	4.9	9.4	24.2	16.8	2.9
Sodium (Na)	mg/L	-	-	127	146	1340	1040	102	1650	1050	11.3	5.4

Guide Limit #1: T1-Soil-Res/Park/Inst/Ind/Com/Commu Property Use

<sup>\*</sup> Please refer to the Reference Information section for an explanation of any qualifiers noted.



L2120222 CONT'D....

Job Reference: 188337

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#### **Saturated Paste Extractables - SOIL**

		Sampl	Lab ID e Date iple ID	L2120222-19 22-JUN-18 BH10 SS2	L2120222-20 22-JUN-18 BH10 SS3	L2120222-21 22-JUN-18 BH10 SS5
Analyte	Unit	Guide #1	Limits #2			
SAR	SAR	2.4	-	17.4	7.40	9.46
Calcium (Ca)	mg/L	-	-	178	113	280
Magnesium (Mg)	mg/L	-	-	32.2	36.1	31.6
Sodium (Na)	mg/L	-	-	960	352	626

Guide Limit #1: T1-Soil-Res/Park/Inst/Ind/Com/Commu Property Use

<sup>\*</sup> Please refer to the Reference Information section for an explanation of any qualifiers noted.



L2120222 CONT'D....

Job Reference: 188337

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**Metals - SOIL** 

ivietais - SUIL												
		Sampl	Lab ID e Date iple ID	L2120222-1 22-JUN-18 BH1 SS2	L2120222-2 22-JUN-18 BH3 SS2	L2120222-3 22-JUN-18 BH2 SS1	L2120222-4 22-JUN-18 BH2 SS2	L2120222-5 22-JUN-18 BH2 SS3	L2120222-6 22-JUN-18 BH4 SS2	L2120222-7 22-JUN-18 BH4 SS3	L2120222-8 22-JUN-18 BH4 SS4	L2120222-9 22-JUN-18 BH5 SS2
Analyte	Unit	Guide #1	Limits #2									
Antimony (Sb)	ug/g	1.3	-	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0
Arsenic (As)	ug/g	18	-	5.8	5.3	4.7	7.9	8.6	6.5	5.1	3.3	3.9
Barium (Ba)	ug/g	220	-	162	91.7	130	81.9	78.8	76.6	156	180	99.0
Beryllium (Be)	ug/g	2.5	-	0.90	0.71	0.95	0.66	0.67	0.59	0.86	1.12	0.73
Boron (B)	ug/g	36	-	8.4	7.3	5.7	8.5	8.5	8.4	14.9	17.2	<5.0
Boron (B), Hot Water Ext.	ug/g	36	-	0.20	0.68	0.55	<0.10	<0.10	<0.10	0.11	0.14	<0.10
Cadmium (Cd)	ug/g	1.2	-	<0.50	<0.50	<0.50	<0.50	<0.50	<0.50	<0.50	<0.50	<0.50
Chromium (Cr)	ug/g	70	-	34.2	25.1	28.9	23.1	23.9	20.6	31.6	37.4	28.6
Cobalt (Co)	ug/g	21	-	19.6	12.9	15.4	12.1	13.9	12.1	15.0	16.0	14.6
Copper (Cu)	ug/g	92	-	28.6	20.7	18.0	35.9	38.7	32.2	25.2	27.2	17.8
Lead (Pb)	ug/g	120	-	15.2	34.1	13.8	10.7	10.6	10.1	10.6	13.7	11.8
Mercury (Hg)	ug/g	0.27	-	0.0365	0.0389	0.0407	0.0185	0.0226	0.0188	0.0139	0.0139	0.0228
Molybdenum (Mo)	ug/g	2	-	<1.0	1.2	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0
Nickel (Ni)	ug/g	82	-	29.9	23.1	25.6	27.8	29.1	25.4	31.1	38.3	26.5
Selenium (Se)	ug/g	1.5	-	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0
Silver (Ag)	ug/g	0.5	-	<0.20	<0.20	<0.20	<0.20	<0.20	<0.20	<0.20	<0.20	<0.20
Thallium (TI)	ug/g	1	-	<0.50	<0.50	<0.50	<0.50	<0.50	<0.50	<0.50	<0.50	<0.50
Uranium (U)	ug/g	2.5	-	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0
Vanadium (V)	ug/g	86	-	43.5	35.1	43.5	32.9	34.1	29.5	43.7	50.0	42.1
Zinc (Zn)	ug/g	290	-	80.1	100	76.3	63.9	66.1	60.5	67.8	77.9	71.6

Guide Limit #1: T1-Soil-Res/Park/Inst/Ind/Com/Commu Property Use

<sup>\*</sup> Please refer to the Reference Information section for an explanation of any qualifiers noted.



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Job Reference: 188337

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Metals - SOIL

		L	ab ID	L2120222-10	L2120222-11	L2120222-12	L2120222-13	L2120222-14	L2120222-15	L2120222-16	L2120222-17	L2120222-18
		Sample		22-JUN-18								
		Sam	ple ID	BH5 SS3	BH5 SS4	BH6 SS2	BH6 SS3	BH6 SS4	BH8 SS2	BH8 SS3	BH8 SS4	BH8 SS5
Analyte	Unit	Guide #1	Limits #2									
Antimony (Sb)	ug/g	1.3	-	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0
Arsenic (As)	ug/g	18	-	6.1	8.0	7.2	7.3	5.9	8.2	5.6	4.0	5.1
Barium (Ba)	ug/g	220	-	44.3	85.5	61.6	55.7	180	96.8	150	130	80.2
Beryllium (Be)	ug/g	2.5	-	<0.50	0.70	0.55	0.54	1.03	0.65	0.89	0.93	0.64
Boron (B)	ug/g	36	-	6.3	8.4	7.7	7.7	16.9	9.2	12.7	14.9	11.5
Boron (B), Hot Water Ext.	ug/g	36	-	<0.10	<0.10	<0.10	<0.10	0.12	<0.10	0.12	0.16	0.12
Cadmium (Cd)	ug/g	1.2	-	<0.50	<0.50	<0.50	<0.50	<0.50	<0.50	<0.50	<0.50	<0.50
Chromium (Cr)	ug/g	70	-	16.5	24.0	19.1	19.2	37.7	24.0	30.2	34.3	24.3
Cobalt (Co)	ug/g	21	-	9.5	13.8	10.8	11.3	21.3	13.9	14.1	15.8	12.0
Copper (Cu)	ug/g	92	-	29.3	31.9	33.4	32.2	31.0	33.6	27.2	29.8	26.4
Lead (Pb)	ug/g	120	-	8.2	9.5	9.1	9.0	13.5	10.0	11.2	13.1	9.5
Mercury (Hg)	ug/g	0.27	-	0.0181	0.0191	0.0189	0.0192	0.0169	0.0195	0.0168	0.0158	0.0110
Molybdenum (Mo)	ug/g	2	-	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0
Nickel (Ni)	ug/g	82	-	20.3	28.5	23.4	24.3	38.4	28.6	31.2	35.9	26.0
Selenium (Se)	ug/g	1.5	-	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0
Silver (Ag)	ug/g	0.5	-	<0.20	<0.20	<0.20	<0.20	<0.20	<0.20	<0.20	<0.20	<0.20
Thallium (TI)	ug/g	1	-	<0.50	<0.50	<0.50	<0.50	<0.50	<0.50	<0.50	<0.50	<0.50
Uranium (U)	ug/g	2.5	-	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	1.1	<1.0
Vanadium (V)	ug/g	86	-	23.5	33.2	27.4	27.7	49.3	33.8	40.3	45.0	34.0
Zinc (Zn)	ug/g	290	-	49.0	63.8	56.0	55.3	86.2	65.3	66.4	80.0	62.1

Guide Limit #1: T1-Soil-Res/Park/Inst/Ind/Com/Commu Property Use

<sup>\*</sup> Please refer to the Reference Information section for an explanation of any qualifiers noted.



L2120222 CONT'D....

Job Reference: 188337

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#### **Metals - SOIL**

			Lab ID	L2120222-19	L2120222-20	L2120222-21
		Sample		22-JUN-18	22-JUN-18	22-JUN-18
		Sam	ple ID	BH10 SS2	BH10 SS3	BH10 SS5
Analyte	Unit	Guide #1	Limits #2			
Antimony (Sb)	ug/g	1.3	-	<1.0	<1.0	<1.0
Arsenic (As)	ug/g	18	-	4.7	3.7	4.1
Barium (Ba)	ug/g	220	-	26.7	19.1	81.8
Beryllium (Be)	ug/g	2.5	-	<0.50	<0.50	0.63
Boron (B)	ug/g	36	-	12.9	14.2	10.7
Boron (B), Hot Water Ext.	ug/g	36	-	0.16	0.15	<0.10
Cadmium (Cd)	ug/g	1.2	-	<0.50	<0.50	<0.50
Chromium (Cr)	ug/g	70	-	11.8	14.0	24.6
Cobalt (Co)	ug/g	21	-	4.7	6.4	13.2
Copper (Cu)	ug/g	92	-	18.2	14.4	24.1
Lead (Pb)	ug/g	120	-	11.2	56.6	9.8
Mercury (Hg)	ug/g	0.27	-	0.0165	0.0234	0.0130
Molybdenum (Mo)	ug/g	2	-	<1.0	<1.0	<1.0
Nickel (Ni)	ug/g	82	-	12.5	15.1	29.3
Selenium (Se)	ug/g	1.5	-	<1.0	<1.0	<1.0
Silver (Ag)	ug/g	0.5	-	<0.20	<0.20	<0.20
Thallium (TI)	ug/g	1	-	<0.50	<0.50	<0.50
Uranium (U)	ug/g	2.5	-	<1.0	<1.0	<1.0
Vanadium (V)	ug/g	86	-	19.1	19.6	35.3
Zinc (Zn)	ug/g	290	-	34.0	37.4	59.6

Guide Limit #1: T1-Soil-Res/Park/Inst/Ind/Com/Commu Property Use

<sup>\*</sup> Please refer to the Reference Information section for an explanation of any qualifiers noted.



L2120222 CONT'D....

Job Reference: 188337

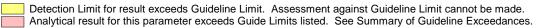
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**Speciated Metals - SOIL** 

openiated inicials ooil											
		Lab II	L2120222-1	L2120222-2	L2120222-3	L2120222-4	L2120222-5	L2120222-6	L2120222-7	L2120222-8	L2120222-9
		Sample Dat	e 22-JUN-18	22-JUN-18	22-JUN-18	22-JUN-18	22-JUN-18	22-JUN-18	22-JUN-18	22-JUN-18	22-JUN-18
		Sample I	D BH1 SS2	BH3 SS2	BH2 SS1	BH2 SS2	BH2 SS3	BH4 SS2	BH4 SS3	BH4 SS4	BH5 SS2
		Guide Limi	s								
Analyte	Unit	#1 #2		_							
		0.66 -									

Guide Limit #1: T1-Soil-Res/Park/Inst/Ind/Com/Commu Property Use



<sup>\*</sup> Please refer to the Reference Information section for an explanation of any qualifiers noted.



L2120222 CONT'D....

Job Reference: 188337

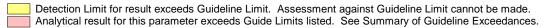
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**Speciated Metals - SOIL** 

		Lak	<b>ID</b> L212022	2-10	L2120222-11	L2120222-12	L2120222-13	L2120222-14	L2120222-15	L2120222-16	L2120222-17	L2120222-18
		Sample D	ate 22-JUN	-18	22-JUN-18							
		Sample	ID BH5 S	S3	BH5 SS4	BH6 SS2	BH6 SS3	BH6 SS4	BH8 SS2	BH8 SS3	BH8 SS4	BH8 SS5
		<b>Guide Lir</b>	nits									
			_									
Analyte	Unit	#1 #	2									

Guide Limit #1: T1-Soil-Res/Park/Inst/Ind/Com/Commu Property Use



<sup>\*</sup> Please refer to the Reference Information section for an explanation of any qualifiers noted.



L2120222 CONT'D....

Job Reference: 188337

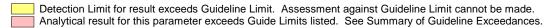
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## **Speciated Metals - SOIL**

		Sample	_ab ID e Date ple ID	L2120222-19 22-JUN-18 BH10 SS2	L2120222-20 22-JUN-18 BH10 SS3	L2120222-21 22-JUN-18 BH10 SS5
Analyte	Unit	Guide #1	Limits #2			
Chromium, Hexavalent	ug/g	0.66		<0.20	<0.20	0.23

#### Guide Limit #1: T1-Soil-Res/Park/Inst/Ind/Com/Commu Property Use



<sup>\*</sup> Please refer to the Reference Information section for an explanation of any qualifiers noted.

#### **Reference Information**

L2120222 CONT'D....
Job Reference: 188337
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**Qualifiers for Individual Parameters Listed:** 

Qualifier Description

SAR:M Reported SAR represents a maximum value. Actual SAR may be lower if both Ca and Mg were detectable.

Methods Listed (if applicable):

ALS Test Code Matrix Test Description Method Reference\*\*

B-HWS-R511-WT Soil Boron-HWE-O.Reg 153/04 (July 2011) HW EXTR, EPA 6010B

A dried solid sample is extracted with calcium chloride, the sample undergoes a heating process. After cooling the sample is filtered and analyzed by ICP/OES.

Analysis conducted in accordance with the Protocol for Analytical Methods Used in the Assessment of Properties under Part XV.1 of the Environmental Protection Act (July 1, 2011).

**CN-WAD-R511-WT** Soil Cyanide (WAD)-O.Reg 153/04 (July MOE 3015/APHA 4500CN I-WAD

The sample is extracted with a strong base for 16 hours, and then filtered. The filtrate is then distilled where the cyanide is converted to cyanogen chloride by reacting with chloramine-T, the cyanogen chloride then reacts with a combination of barbituric acid and isonicotinic acid to form a highly colored complex.

Analysis conducted in accordance with the Protocol for Analytical Methods Used in the Assessment of Properties under Part XV.1 of the Environmental Protection Act (July 1, 2011).

CR-CR6-IC-WT Soil Hexavalent Chromium in Soil SW846 3060A/7199

This analysis is carried out using procedures adapted from "Test Methods for Evaluating Solid Waste" SW-846, Method 7199, published by the United States Environmental Protection Agency (EPA). The procedure involves analysis for chromium (VI) by ion chromatography using diphenylcarbazide in a sulphuric acid solution.

Analysis conducted in accordance with the Protocol for Analytical Methods Used in the Assessment of Properties under Part XV.1 of the Environmental Protection Act (July 1, 2011).

EC-WT Soil Conductivity (EC) MOEE E3138

A representative subsample is tumbled with de-ionized (DI) water. The ratio of water to soil is 2:1 v/w. After tumbling the sample is then analyzed by a conductivity meter.

Analysis conducted in accordance with the Protocol for Analytical Methods Used in the Assessment of Properties under Part XV.1 of the Environmental Protection Act (July 1, 2011).

HG-200.2-CVAA-WT Soil Mercury in Soil by CVAAS EPA 200.2/1631E (mod)

Soil samples are digested with nitric and hydrochloric acids, followed by analysis by CVAAS.

Analysis conducted in accordance with the Protocol for Analytical Methods Used in the Assessment of Properties under Part XV.1 of the Environmental Protection Act (July 1, 2011).

MET-200.2-CCMS-WT Soil Metals in Soil by CRC ICPMS EPA 200.2/6020A (mod)

This method uses a heated strong acid digestion with HNO3 and HCl and is intended to liberate metals that may be environmentally available. Silicate minerals are not solubilized. Dependent on sample matrix, some metals may be only partially recovered, including Al, Ba, Be, Cr, Sr, Ti, Tl, V, W, and Zr. Volatile forms of sulfur (including sulfide) may not be captured, as they may be lost during sampling, storage, or digestion. Analysis is by Collision/Reaction Cell ICPMS.

Analysis conducted in accordance with the Protocol for Analytical Methods Used in the Assessment of Properties under Part XV.1 of the Environmental Protection Act (July 1, 2011), unless a subset of the Analytical Test Group (ATG) has been requested (the Protocol states that all analytes in an ATG must be reported).

MOISTURE-WT Soil % Moisture Gravimetric: Oven Dried

PH-WT Soil pH MOEE E3137A

#### **Reference Information**

L2120222 CONT'D....
Job Reference: 188337
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Methods Listed (if applicable):

ALS Test Code Matrix Test Description Method Reference\*\*

A minimum 10g portion of the sample is extracted with 20mL of 0.01M calcium chloride solution by shaking for at least 30 minutes. The aqueous layer is separated from the soil and then analyzed using a pH meter and electrode.

Analysis conducted in accordance with the Protocol for Analytical Methods Used in the Assessment of Properties under Part XV.1 of the Environmental Protection Act (July 1, 2011).

SAR-R511-WT

Soil

SAR-O.Reg 153/04 (July 2011)

SW846 6010C

A dried, disaggregated solid sample is extracted with deionized water, the aqueous extract is separated from the solid, acidified and then analyzed using a ICP/OES. The concentrations of Na, Ca and Mg are reported as per CALA requirements for calculated parameters. These individual parameters are not for comparison to any guideline.

Analysis conducted in accordance with the Protocol for Analytical Methods Used in the Assessment of Properties under Part XV.1 of the Environmental Protection Act (July 1, 2011).

\*\*ALS test methods may incorporate modifications from specified reference methods to improve performance.

Chain of Custody Numbers:

The last two letters of the above test code(s) indicate the laboratory that performed analytical analysis for that test. Refer to the list below:

Laboratory Definition Code

Laboratory Location

WT

ALS ENVIRONMENTAL - WATERLOO, ONTARIO, CANADA

#### **GLOSSARY OF REPORT TERMS**

Surrogates are compounds that are similar in behaviour to target analyte(s), but that do not normally occur in environmental samples. For applicable tests, surrogates are added to samples prior to analysis as a check on recovery. In reports that display the D.L. column, laboratory objectives for surrogates are listed there.

mg/kg - milligrams per kilogram based on dry weight of sample

mg/kg wwt - milligrams per kilogram based on wet weight of sample

mg/kg lwt - milligrams per kilogram based on lipid-adjusted weight

mg/L - unit of concentration based on volume, parts per million.

< - Less than.

D.L. - The reporting limit.

N/A - Result not available. Refer to qualifier code and definition for explanation.

Test results reported relate only to the samples as received by the laboratory.

UNLESS OTHERWISE STATED, ALL SAMPLES WERE RECEIVED IN ACCEPTABLE CONDITION.

Analytical results in unsigned test reports with the DRAFT watermark are subject to change, pending final QC review.

Application of guidelines is provided "as is" without warranty of any kind, either expressed or implied, including, but not limited to fitness for a particular purpose, or non-infringement. ALS assumes no responsibility for errors or omissions in the information.



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Client: Soil Mat Engineers & Consulting Ltd. (Hamilton)

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Test	Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
B-HWS-R511-WT	Soil							
Batch R4110400 WG2812102-4 DUP Boron (B), Hot Water Ex	ĸt.	<b>L2121112-4</b> 0.33	0.31		ug/g	5.8	30	03-JUL-18
WG2812102-2 IRM Boron (B), Hot Water Ex	ct.	HOTB-SAL_SO	<b>DIL5</b> 91.9		%		70-130	03-JUL-18
WG2812102-3 LCS Boron (B), Hot Water Ex	ct.		107.3		%		70-130	03-JUL-18
WG2812102-1 MB Boron (B), Hot Water Ex	ct.		<0.10		ug/g		0.1	03-JUL-18
Batch R4112089 WG2811007-4 DUP Boron (B), Hot Water Ex	ct.	<b>L2120222-11</b> <0.10	<0.10	RPD-NA	ug/g	N/A	30	03-JUL-18
WG2811007-2 IRM Boron (B), Hot Water Ex	xt.	HOTB-SAL_S	<b>DIL5</b> 100.2		%		70-130	03-JUL-18
WG2811007-3 LCS Boron (B), Hot Water Ex	ct.		108.5		%		70-130	03-JUL-18
<b>WG2811007-1 MB</b> Boron (B), Hot Water Ex	ct.		<0.10		ug/g		0.1	03-JUL-18
Batch R4112108 WG2812103-4 DUP Boron (B), Hot Water Ex	ct.	<b>L2120250-2</b> <0.10	<0.10	RPD-NA	ug/g	N/A	30	03-JUL-18
WG2812103-2 IRM Boron (B), Hot Water Ex	ct.	HOTB-SAL_S	<b>DIL5</b> 92.0		%		70-130	03-JUL-18
WG2812103-3 LCS Boron (B), Hot Water Ex	ct.		110.2		%		70-130	03-JUL-18
WG2812103-1 MB Boron (B), Hot Water Ex	ct.		<0.10		ug/g		0.1	03-JUL-18
CN-WAD-R511-WT Batch R4110089	Soil							
WG2810320-3 DUP Cyanide, Weak Acid Dis	s	<b>L2120222-1</b> <0.050	<0.050	RPD-NA	ug/g	N/A	35	03-JUL-18
WG2810479-3 DUP Cyanide, Weak Acid Dis	s	<b>L2120250-2</b> <0.050	<0.050	RPD-NA	ug/g	N/A	35	03-JUL-18
WG2810320-2 LCS Cyanide, Weak Acid Dis	s		93.4		%		80-120	03-JUL-18
WG2810479-2 LCS Cyanide, Weak Acid Dis	s		94.3		%		80-120	03-JUL-18
<b>WG2810320-1 MB</b> Cyanide, Weak Acid Dis	s		<0.050		ug/g		0.05	03-JUL-18



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Client: Soil Mat Engineers & Consulting Ltd. (Hamilton)

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Test	Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
CN-WAD-R511-WT  Batch R4110089  WG2810479-1 MB	Soil							
Cyanide, Weak Acid Dis	S		<0.050		ug/g		0.05	03-JUL-18
WG2810320-4 MS Cyanide, Weak Acid Dis	s	L2120222-1	102.2		%		70-130	03-JUL-18
WG2810479-4 MS Cyanide, Weak Acid Dis	s	L2120250-2	98.3		%		70-130	03-JUL-18
CR-CR6-IC-WT	Soil							
Batch R4104042		WT 000010						
WG2809723-4 CRM Chromium, Hexavalent		WT-SQC012	87.8		%		70-130	29-JUN-18
WG2809723-3 DUP Chromium, Hexavalent		<b>L2119759-4</b> <0.20	<0.20	RPD-NA	ug/g	N/A	35	29-JUN-18
WG2809723-2 LCS Chromium, Hexavalent			94.9		%		80-120	29-JUN-18
WG2809723-1 MB Chromium, Hexavalent			<0.20		ug/g		0.2	29-JUN-18
Batch R4109452								
WG2809902-4 CRM Chromium, Hexavalent		WT-SQC012	88.6		%		70-130	03-JUL-18
WG2809902-3 DUP Chromium, Hexavalent		<b>L2120222-8</b> <0.20	<0.20	RPD-NA	ug/g	N/A	35	03-JUL-18
WG2809902-2 LCS Chromium, Hexavalent			100.0		%		80-120	03-JUL-18
WG2809902-1 MB Chromium, Hexavalent			<0.20		ug/g		0.2	03-JUL-18
EC-WT	Soil							
Batch R4110550								
WG2812107-4 DUP Conductivity		<b>WG2812107-3</b> 0.140	0.132		mS/cm	5.5	20	03-JUL-18
WG2812347-1 LCS Conductivity			98.5		%		90-110	03-JUL-18
WG2812107-1 MB Conductivity			<0.0040		mS/cm		0.004	03-JUL-18
Batch R4110552 WG2811033-4 DUP Conductivity		<b>WG2811033-3</b> 1.68	1.50		mS/cm	11	20	03-JUL-18
WG2812346-1 LCS								



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Client: Soil Mat Engineers & Consulting Ltd. (Hamilton)

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Test	Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
EC-WT	Soil							
Batch R4110 WG2812346-1 LC Conductivity			100.0		%		90-110	03-JUL-18
WG2811033-1 MI Conductivity	В		<0.0040		mS/cm		0.004	03-JUL-18
HG-200.2-CVAA-WT	Soil							
Batch R4110 WG2810978-2 CF Mercury (Hg)	323 RM	WT-CANMET-	<b>ΓΙLL1</b> 101.3		%		70-130	03-JUL-18
WG2812091-2 CF Mercury (Hg)	RM	WT-CANMET-1	<b>ΓΙLL1</b> 101.1		%		70-130	03-JUL-18
WG2812092-2 CF Mercury (Hg)	RM	WT-CANMET-	<b>ΓΙLL1</b> 103.1		%		70-130	03-JUL-18
WG2810978-6 DU Mercury (Hg)	JP	<b>WG2810978-5</b> 0.0956	0.0962		ug/g	0.7	40	03-JUL-18
WG2812091-6 DU Mercury (Hg)	JP	<b>WG2812091-5</b> 0.0181	0.0175		ug/g	3.4	40	03-JUL-18
WG2812092-6 DU Mercury (Hg)	JP	<b>WG2812092-5</b> 0.0192	0.0191		ug/g	0.8	40	03-JUL-18
<b>WG2810978-3 LC</b> Mercury (Hg)	cs		107.0		%		80-120	03-JUL-18
<b>WG2812091-3 LC</b> Mercury (Hg)	cs		103.0		%		80-120	03-JUL-18
<b>WG2812092-3 LC</b> Mercury (Hg)	CS		105.0		%		80-120	03-JUL-18
WG2810978-1 MI Mercury (Hg)	В		<0.0050		mg/kg		0.005	03-JUL-18
WG2812091-1 MI Mercury (Hg)			<0.0050		mg/kg		0.005	03-JUL-18
WG2812092-1 Mi Mercury (Hg)	В		<0.0050		mg/kg		0.005	03-JUL-18
MET-200.2-CCMS-WT	Soil							
Batch R4111 WG2812091-2 CF Antimony (Sb)	872 RM	WT-CANMET-	<b>ΓΙLL1</b> 98.0		%		70-130	03-JUL-18
Arsenic (As)			104.4		%		70-130	03-JUL-18
Barium (Ba)			103.2		%		70-130	03-JUL-18
Beryllium (Be)			92.6		%		70-130	03-JUL-18



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Client: Soil Mat Engineers & Consulting Ltd. (Hamilton)

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Test	Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
MET-200.2-CCMS-WT	Soil							
Batch R4111872	2							
WG2812091-2 CRM		WT-CANMET-						
Boron (B)			2.7		mg/kg		0-8.2	03-JUL-18
Cadmium (Cd)			101.7		%		70-130	03-JUL-18
Chromium (Cr)			100.8		%		70-130	03-JUL-18
Cobalt (Co)			103.1		%		70-130	03-JUL-18
Copper (Cu)			104.3		%		70-130	03-JUL-18
Lead (Pb)			100.6		%		70-130	03-JUL-18
Molybdenum (Mo)			98.0		%		70-130	03-JUL-18
Nickel (Ni)			102.2		%		70-130	03-JUL-18
Selenium (Se)			0.27		mg/kg		0.11-0.51	03-JUL-18
Silver (Ag)			0.23		mg/kg		0.13-0.33	03-JUL-18
Thallium (TI)			0.118		mg/kg		0.077-0.18	03-JUL-18
Uranium (U)			102.5		%		70-130	03-JUL-18
Vanadium (V)			100.6		%		70-130	03-JUL-18
Zinc (Zn)			102.1		%		70-130	03-JUL-18
WG2812091-6 DUP Antimony (Sb)		<b>WG2812091-5</b> 0.13	0.14		ug/g	9.8	30	03-JUL-18
Arsenic (As)		6.08	6.82		ug/g	12	30	03-JUL-18
Barium (Ba)		44.3	49.4		ug/g	11	40	03-JUL-18
Beryllium (Be)		0.43	0.54		ug/g	23	30	03-JUL-18
Boron (B)		6.3	7.7		ug/g	20	30	03-JUL-18
Cadmium (Cd)		0.078	0.094		ug/g	18	30	03-JUL-18
Chromium (Cr)		16.5	18.3		ug/g	10	30	03-JUL-18
Cobalt (Co)		9.48	10.8		ug/g	13	30	03-JUL-18
Copper (Cu)		29.3	33.0		ug/g	12	30	03-JUL-18
Lead (Pb)		8.22	8.92		ug/g	8.1	40	03-JUL-18
Molybdenum (Mo)		0.36	0.39		ug/g	9.0	40	03-JUL-18
Nickel (Ni)		20.3	22.7		ug/g	12	30	03-JUL-18
Selenium (Se)		<0.20	<0.20	RPD-NA	ug/g	N/A	30	03-JUL-18
Silver (Ag)		<0.10	<0.10	RPD-NA	ug/g	N/A	40	03-JUL-18
Thallium (TI)		0.086	0.099		ug/g	13	30	03-JUL-18
Uranium (U)		0.469	0.522		ug/g	11	30	03-JUL-18
Vanadium (V)		23.5	27.6		ug/g	16	30	03-JUL-18
Zinc (Zn)		49.0	55.6		ug/g	13	30	03-JUL-18
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Client: Soil Mat Engineers & Consulting Ltd. (Hamilton)

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Metr-2002-CCMS-WT   Soil	Test	Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
WG8212091-4         LCS           Artmony (Sb)         106.6         %         80-120         03-JUL-18           Arsenic (As)         102.4         %         80-120         03-JUL-18           Barlum (Ba)         101.3         %         80-120         03-JUL-18           Benylium (Be)         90.2         %         80-120         03-JUL-18           Boron (B)         87.8         %         80-120         03-JUL-18           Cadmium (Cd)         101.3         %         80-120         03-JUL-18           Chromium (Cd)         99.8         %         80-120         03-JUL-18           Cobalt (Co)         99.8         %         80-120         03-JUL-18           Ced (Co)         99.8         %         80-120         03-JUL-18           Lead (Pb)         101.9         %         80-120         03-JUL-18           Lead (Pb)         101.9         %         80-120         03-JUL-18           Nickel (Ni)         99.87         %         80-120         03-JUL-18           Nickel (Ni)         99.57         %         80-120         03-JUL-18           Silver (Ag)         100.4         %         80-120         03-JUL-18	MET-200.2-CCMS-WT	Soil							
Animony (Sb)         106.6         %         80-120         03-JUL-18           Arsenic (As)         102.4         %         80-120         03-JUL-18           Barium (Ba)         101.3         %         80-120         03-JUL-18           Beryllium (Be)         90.2         %         80-120         03-JUL-18           Boron (B)         87.8         %         80-120         03-JUL-18           Cadmium (Cd)         101.3         %         80-120         03-JUL-18           Chromium (Cr)         99.8         %         80-120         03-JUL-18           Cobalt (Co)         99.7         %         80-120         03-JUL-18           Copper (Cu)         99.8         %         80-120         03-JUL-18           Lead (Pb)         101.9         %         80-120         03-JUL-18           Molybdenum (Mo)         98.1         %         80-120         03-JUL-18           Nickel (Ni)         99.97         %         80-120         03-JUL-18           Selenium (Se)         102.5         %         80-120         03-JUL-18           Selverium (Se)         100.4         %         80-120         03-JUL-18           Thallium (Ti)         98.4	Batch R4111872								
Arsenic (As) 102.4 % 80-120 03-JUL-18 Barium (Ba) 101.3 % 80-120 03-JUL-18 Beryllium (Be) 90.2 % 80-120 03-JUL-18 Boron (B) 87.8 % 80-120 03-JUL-18 Cadmium (Cd) 101.3 % 80-120 03-JUL-18 Cadmium (Cd) 101.3 % 80-120 03-JUL-18 Chromium (Cr) 99.8 % 80-120 03-JUL-18 Cobalt (Co) 99.7 % 80-120 03-JUL-18 Copper (Cd) 99.8 % 80-120 03-JUL-18 Lead (Pb) 101.9 % 80-120 03-JUL-18 Molybdenum (Mo) 98.1 % 80-120 03-JUL-18 Nickel (Ni) 99.97 % 80-120 03-JUL-18 Silver (Ag) 100.4 % 80-120 03-JUL-18 Silver (Ag) 100.4 % 80-120 03-JUL-18 Cilver (A									
Barium (Ba)         101.3         %         80-120         03-JUL-18           Baryllum (Be)         90.2         %         80-120         03-JUL-18           Boron (B)         87.8         %         80-120         03-JUL-18           Cadmium (Cd)         101.3         %         80-120         03-JUL-18           Chromium (Cr)         99.8         %         80-120         03-JUL-18           Cobalt (Co)         99.7         %         80-120         03-JUL-18           Copper (Cu)         98.8         %         80-120         03-JUL-18           Lead (Pb)         101.9         %         80-120         03-JUL-18           Lead (Pb)         101.9         %         80-120         03-JUL-18           Nickel (Ni)         99.97         %         80-120         03-JUL-18           Nickel (Ni)         99.97         %         80-120         03-JUL-18           Selenium (Se)         102.5         %         80-120         03-JUL-18           Silver (Ag)         100.4         %         80-120         03-JUL-18           Uranium (U)         102.6         %         80-120         03-JUL-18           Uranium (V)         103.5         %									
Beryllium (Be)         90.2         %         80-120         03-JUL-18           Boron (B)         87.8         %         80-120         03-JUL-18           Cadmium (Cd)         101.3         %         80-120         03-JUL-18           Chromium (Cr)         99.8         %         80-120         03-JUL-18           Cobalt (Co)         99.7         %         80-120         03-JUL-18           Copper (Cu)         99.8         %         80-120         03-JUL-18           Lead (Pb)         101.9         %         80-120         03-JUL-18           Molybdenum (Mo)         98.1         %         80-120         03-JUL-18           Nickel (Ni)         99.97         %         80-120         03-JUL-18           Silver (Ag)         102.5         %         80-120         03-JUL-18           Silver (Ag)         100.4         %         80-120         03-JUL-18           Vanadium (U)         102.6         %         80-120         03-JUL-18           Vanadium (V)         103.5         %         80-120         03-JUL-18           Vanadium (V)         103.5         %         80-120         03-JUL-18           Vanadium (V)         103.5									
Boron (B)         87.8         %         80-120         03-JUL-18           Cadmium (Cd)         101.3         %         80-120         03-JUL-18           Chromium (Cr)         99.8         %         80-120         03-JUL-18           Cobalt (Co)         99.7         %         80-120         03-JUL-18           Copper (Cu)         99.8         %         80-120         03-JUL-18           Lead (Pb)         101.9         %         80-120         03-JUL-18           Molybdenum (Mo)         98.1         %         80-120         03-JUL-18           Nickel (Ni)         99.97         %         80-120         03-JUL-18           Silver (Ag)         100.4         %         80-120         03-JUL-18           Silver (Ag)         100.4         %         80-120         03-JUL-18           Thallium (TI)         98.4         %         80-120         03-JUL-18           Thallium (TI)         102.6         %         80-120         03-JUL-18           Vanadium (V)         103.5         %         80-120         03-JUL-18           Variatium (J         102.6         %         80-120         03-JUL-18           WG2812091-1         MB         <									
Cadmium (Cd)         101.3         %         80-120         03-JUL-18           Chromium (Cr)         99.8         %         80-120         03-JUL-18           Cobalt (Co)         99.7         %         80-120         03-JUL-18           Copper (Cu)         99.8         %         80-120         03-JUL-18           Lead (Pb)         101.9         %         80-120         03-JUL-18           Molybdenum (Mo)         98.1         %         80-120         03-JUL-18           Nickel (Ni)         99.97         %         80-120         03-JUL-18           Selenium (Se)         102.5         %         80-120         03-JUL-18           Selenium (Se)         102.5         %         80-120         03-JUL-18           Thallium (TI)         98.4         %         80-120         03-JUL-18           Thallium (U)         102.6         %         80-120         03-JUL-18           Uranium (U)         102.5         %         80-120         03-JUL-18           Vanadium (V)         103.5         %         80-120         03-JUL-18           WG2812091-1         MB           Anterior (Zn)         0.0         0.0         mg/kg         0.1         <								80-120	03-JUL-18
Chromium (Cr)         99.8         %         80-120         03-JUL-18           Cobalt (Co)         99.7         %         80-120         03-JUL-18           Copper (Cu)         99.8         %         80-120         03-JUL-18           Lead (Pb)         101.9         %         80-120         03-JUL-18           Molybdenum (Mo)         98.1         %         80-120         03-JUL-18           Nickel (Ni)         99.97         %         80-120         03-JUL-18           Silver (Ag)         102.5         %         80-120         03-JUL-18           Silver (Ag)         100.4         %         80-120         03-JUL-18           Vanadium (V)         102.5         %         80-120         03-JUL-18           Vanadium (V)         103.5         %         80-120         03-JUL-18           Zinc (Zn)         95.0         %         80-120         03-JUL-18           WG281209-1         MB         Ar									
Cobalt (Co)         99.7         %         80-120         03-JUL-18           Copper (Cu)         99.8         %         80-120         03-JUL-18           Lead (Pb)         101.9         %         80-120         03-JUL-18           Molybdenum (Mo)         98.1         %         80-120         03-JUL-18           Nickel (Ni)         99.97         %         80-120         03-JUL-18           Selenium (Se)         102.5         %         80-120         03-JUL-18           Silver (Ag)         100.4         %         80-120         03-JUL-18           Thallium (Tl)         98.4         %         80-120         03-JUL-18           Uranium (U)         102.6         %         80-120         03-JUL-18           Vanadium (V)         103.5         %         80-120         03-JUL-18           WG2812091-1         MB         MB         7         7         7         80-120         03-JUL-18								80-120	03-JUL-18
Copper (Cu)         99.8         %         80-120         03-JUL-18           Lead (Pb)         101.9         %         80-120         03-JUL-18           Molybdenum (Mo)         98.1         %         80-120         03-JUL-18           Nickel (Ni)         99.97         %         80-120         03-JUL-18           Selenium (Se)         102.5         %         80-120         03-JUL-18           Silver (Ag)         100.4         %         80-120         03-JUL-18           Thallium (TI)         98.4         %         80-120         03-JUL-18           Uranium (U)         102.6         %         80-120         03-JUL-18           Vanadium (V)         103.5         %         80-120         03-JUL-18           Vanadium (V)         0.0								80-120	03-JUL-18
Lead (Pb)       101.9       %       80-120       03-JUL-18         Molybdenum (Mo)       98.1       %       80-120       03-JUL-18         Nickel (Ni)       99.97       %       80-120       03-JUL-18         Selenium (Se)       102.5       %       80-120       03-JUL-18         Silver (Ag)       100.4       %       80-120       03-JUL-18         Thallium (TI)       98.4       %       80-120       03-JUL-18         Uranium (U)       102.6       %       80-120       03-JUL-18         Vanaddum (V)       103.5       %       80-120       03-JUL-18         Zinc (Zn)       95.0       %       80-120       03-JUL-18         WG2812091-1       MB       Martimony (Sb)       <0.10						%		80-120	03-JUL-18
Molybdenum (Mo)         98.1         %         80-120         03-JUL-18           Nickel (Ni)         99.97         %         80-120         03-JUL-18           Selenium (Se)         102.5         %         80-120         03-JUL-18           Silver (Ag)         100.4         %         80-120         03-JUL-18           Thallium (TI)         98.4         %         80-120         03-JUL-18           Uranium (U)         103.5         %         80-120         03-JUL-18           Vanadium (V)         103.5         %         80-120         03-JUL-18           Zinc (Zn)         95.0         %         80-120         03-JUL-18           WG2812091-1         MB         MB         40.10         mg/kg         0.1         03-JUL-18           WG2812091-1         MB          <0.10								80-120	03-JUL-18
Nickel (Ni)         99.97         %         80-120         03-JUL-18           Selenium (Se)         102.5         %         80-120         03-JUL-18           Silver (Ag)         100.4         %         80-120         03-JUL-18           Thallium (TI)         98.4         %         80-120         03-JUL-18           Uranium (U)         102.6         %         80-120         03-JUL-18           Vanadium (V)         103.5         %         80-120         03-JUL-18           Zinc (Zn)         95.0         %         80-120         03-JUL-18           Zinc (Zn)         95.0         %         80-120         03-JUL-18           Zinc (Zn)         95.0         %         80-120         03-JUL-18           WG2812091-1         MB         Name         0.1         03-JUL-18           Arsenic (As)         <0.10				101.9				80-120	03-JUL-18
Selenium (Se)         102.5         %         80-120         03-JUL-18           Silver (Ag)         100.4         %         80-120         03-JUL-18           Thallium (TI)         98.4         %         80-120         03-JUL-18           Uranium (U)         102.6         %         80-120         03-JUL-18           Vanadium (V)         103.5         %         80-120         03-JUL-18           Zinc (Zn)         95.0         %         80-120         03-JUL-18           WG2812091-1         MB         Nantimony (Sb)         <0.10	Molybdenum (Mo)					%		80-120	03-JUL-18
Silver (Ag)       100.4       %       80-120       03-JUL-18         Thallium (TI)       98.4       %       80-120       03-JUL-18         Uranium (U)       102.6       %       80-120       03-JUL-18         Vanadium (V)       103.5       %       80-120       03-JUL-18         Zinc (Zn)       95.0       %       80-120       03-JUL-18         WG2812091-1       MB         Antimony (Sb)       <0.10	Nickel (Ni)			99.97		%		80-120	03-JUL-18
Thallium (TI)         98.4         %         80-120         03-JUL-18           Uranium (U)         102.6         %         80-120         03-JUL-18           Vanadium (V)         103.5         %         80-120         03-JUL-18           Zinc (Zn)         95.0         %         80-120         03-JUL-18           WG2812091-1         MB         NB         VANDER (SI)         VANDER (SI) <td< td=""><td>Selenium (Se)</td><td></td><td></td><td>102.5</td><td></td><td>%</td><td></td><td>80-120</td><td>03-JUL-18</td></td<>	Selenium (Se)			102.5		%		80-120	03-JUL-18
Uranium (U)         102.6         %         80-120         03-JUL-18           Vanadium (V)         103.5         %         80-120         03-JUL-18           Zinc (Zn)         95.0         %         80-120         03-JUL-18           WG2812091-1 MB         MB         Variance	Silver (Ag)			100.4		%		80-120	03-JUL-18
Vanadium (V)         103.5         %         80-120         03-JUL-18           Zinc (Zn)         95.0         %         80-120         03-JUL-18           WG2812091-1 MB           Antimony (Sb)         < 0.10         mg/kg         0.1         03-JUL-18           Arsenic (As)         < 0.10         mg/kg         0.1         03-JUL-18           Barium (Ba)         < 0.50         mg/kg         0.5         03-JUL-18           Beryllium (Be)         < 0.10         mg/kg         0.1         03-JUL-18           Boron (B)         < 5.0         mg/kg         0.1         03-JUL-18           Cadmium (Cd)         < 0.020         mg/kg         0.5         03-JUL-18           Chromium (Cr)         < 0.50         mg/kg         0.5         03-JUL-18           Cobalt (Co)         < 0.10         mg/kg         0.5         03-JUL-18           Copper (Cu)         < 0.50         mg/kg         0.5         03-JUL-18           Lead (Pb)         < 0.50         mg/kg         0.5         03-JUL-18           Molybdenum (Mo)         < 0.10         mg/kg         0.5         03-JUL-18           Nickel (Ni)         < 0.50         mg/kg         0.5         0	Thallium (TI)			98.4		%		80-120	03-JUL-18
Zinc (Zn)         95.0         %         80-120         03-JUL-18           WG2812091-1         MB         Co.10         mg/kg         0.1         03-JUL-18           Arsenic (As)         <0.10         mg/kg         0.1         03-JUL-18           Barium (Ba)         <0.50         mg/kg         0.5         03-JUL-18           Beryllium (Be)         <0.10         mg/kg         0.1         03-JUL-18           Boron (B)         <5.0         mg/kg         5         03-JUL-18           Cadmium (Cd)         <0.020         mg/kg         0.5         03-JUL-18           Chromium (Cr)         <0.50         mg/kg         0.5         03-JUL-18           Cobalt (Co)         <0.10         mg/kg         0.5         03-JUL-18           Copper (Cu)         <0.50         mg/kg         0.5         03-JUL-18           Lead (Pb)         <0.50         mg/kg         0.5         03-JUL-18           Molybdenum (Mo)         <0.10         mg/kg         0.5         03-JUL-18           Selenium (Se)         <0.20         mg/kg         0.2         03-JUL-18           Silver (Ag)         <0.10         mg/kg         0.1         03-JUL-18	Uranium (U)			102.6		%		80-120	03-JUL-18
WG2812091-1 Antimony (Sb)         MB           Antimony (Sb)         <0.10	Vanadium (V)			103.5		%		80-120	03-JUL-18
Antimony (Sb)       <0.10	Zinc (Zn)			95.0		%		80-120	03-JUL-18
Arsenic (As)       <0.10									
Barium (Ba)       <0.50									
Beryllium (Be)       <0.10				<0.10		mg/kg		0.1	03-JUL-18
Boron (B)       <5.0				<0.50		mg/kg		0.5	03-JUL-18
Cadmium (Cd)       <0.020	, , ,			<0.10		mg/kg		0.1	03-JUL-18
Chromium (Cr)       <0.50       mg/kg       0.5       03-JUL-18         Cobalt (Co)       <0.10				<5.0		mg/kg		5	03-JUL-18
Cobalt (Co)       <0.10	` ,			<0.020		mg/kg		0.02	03-JUL-18
Copper (Cu)       <0.50	Chromium (Cr)			< 0.50		mg/kg		0.5	03-JUL-18
Lead (Pb)       <0.50	Cobalt (Co)			<0.10		mg/kg		0.1	03-JUL-18
Molybdenum (Mo)       <0.10	Copper (Cu)			< 0.50		mg/kg		0.5	03-JUL-18
Nickel (Ni)       <0.50       mg/kg       0.5       03-JUL-18         Selenium (Se)       <0.20	Lead (Pb)			< 0.50		mg/kg		0.5	03-JUL-18
Selenium (Se)       <0.20       mg/kg       0.2       03-JUL-18         Silver (Ag)       <0.10	Molybdenum (Mo)			<0.10		mg/kg		0.1	03-JUL-18
Silver (Ag) <0.10 mg/kg 0.1 03-JUL-18	Nickel (Ni)			<0.50		mg/kg		0.5	03-JUL-18
	Selenium (Se)			<0.20		mg/kg		0.2	03-JUL-18
Thallium (TI) <0.050 mg/kg 0.05 03-JUL-18	Silver (Ag)			<0.10		mg/kg		0.1	03-JUL-18
	Thallium (TI)			<0.050		mg/kg		0.05	03-JUL-18



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Client: Soil Mat Engineers & Consulting Ltd. (Hamilton)

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Test		Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
MET-200.2-CCMS-\	ΝΤ	Soil							
Batch R4	111872								
WG2812091-1	MB			-0.050		ma/l:~		0.05	00 1111 45
Uranium (U) Vanadium (V)				<0.050		mg/kg		0.05	03-JUL-18
				<0.20 <2.0		mg/kg		2	03-JUL-18
Zinc (Zn)				<2.0		mg/kg		2	03-JUL-18
Batch R4: WG2812092-2	111909 CRM		WT-CANMET	TU 1 4					
Antimony (Sb)	CKIVI		WI-CANWEI	111.9		%		70-130	03-JUL-18
Arsenic (As)				119.5		%		70-130	03-JUL-18
Barium (Ba)				119.9		%		70-130	03-JUL-18
Beryllium (Be)				95.8		%		70-130	03-JUL-18
Boron (B)				3.1		mg/kg		0-8.2	03-JUL-18
Cadmium (Cd)				118.7		%		70-130	03-JUL-18
Chromium (Cr)				115.7		%		70-130	03-JUL-18
Cobalt (Co)				118.1		%		70-130	03-JUL-18
Copper (Cu)				120.0		%		70-130	03-JUL-18
Lead (Pb)				113.2		%		70-130	03-JUL-18
Molybdenum (M	lo)			106.8		%		70-130	03-JUL-18
Nickel (Ni)				118.0		%		70-130	03-JUL-18
Selenium (Se)				0.39		mg/kg		0.11-0.51	03-JUL-18
Silver (Ag)				0.26		mg/kg		0.13-0.33	03-JUL-18
Thallium (TI)				0.141		mg/kg		0.077-0.18	03-JUL-18
Uranium (U)				115.0		%		70-130	03-JUL-18
Vanadium (V)				118.9		%		70-130	03-JUL-18
Zinc (Zn)				119.7		%		70-130	03-JUL-18
WG2812092-6	DUP		<b>WG2812092-</b> 0.14	<b>5</b> 0.12		ua/a	40	20	00 1111 40
Antimony (Sb)						ug/g	18	30	03-JUL-18
Arsenic (As) Barium (Ba)			7.33 55.7	5.92 44.6		ug/g	21	30	03-JUL-18
Beryllium (Be)						ug/g	22	40	03-JUL-18
Boron (B)			0.54	0.42		ug/g	24	30	03-JUL-18
			7.7	6.3		ug/g	21	30	03-JUL-18
Cadmium (Cd)			0.080	0.073		ug/g	8.8	30	03-JUL-18
Chromium (Cr)			19.2	15.5		ug/g	22	30	03-JUL-18
Cobalt (Co)			11.3	9.08		ug/g	22	30	03-JUL-18
Copper (Cu)			32.2	26.1		ug/g	21	30	03-JUL-18
Lead (Pb)			9.00	7.50		ug/g	18	40	03-JUL-18



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Client: Soil Mat Engineers & Consulting Ltd. (Hamilton)

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Test	Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
MET-200.2-CCMS-WT	Soil							
Batch R4111909								
WG2812092-6 DUP		WG2812092-						
Molybdenum (Mo)		0.40	0.33		ug/g	19	40	03-JUL-18
Nickel (Ni)		24.3	19.5		ug/g	22	30	03-JUL-18
Selenium (Se)		<0.20	<0.20	RPD-NA	ug/g	N/A	30	03-JUL-18
Silver (Ag)		<0.10	<0.10	RPD-NA	ug/g	N/A	40	03-JUL-18
Thallium (TI)		0.093	0.072		ug/g	26	30	03-JUL-18
Uranium (U)		0.603	0.512		ug/g	16	30	03-JUL-18
Vanadium (V)		27.7	22.3		ug/g	22	30	03-JUL-18
Zinc (Zn)		55.3	44.5		ug/g	22	30	03-JUL-18
<b>WG2812092-4 LCS</b> Antimony (Sb)			111.7		%		80-120	03-JUL-18
Arsenic (As)			116.8		%		80-120	03-JUL-18
Barium (Ba)			114.8		%		80-120	03-JUL-18
Beryllium (Be)			101.0		%		80-120	03-JUL-18
Boron (B)			95.1		%		80-120	03-JUL-18
Cadmium (Cd)			108.1		%		80-120	03-JUL-18
Chromium (Cr)			113.5		%		80-120	03-JUL-18
Cobalt (Co)			113.3		%		80-120	03-JUL-18
Copper (Cu)			112.6		%		80-120	03-JUL-18
Lead (Pb)			111.2		%		80-120	03-JUL-18
Molybdenum (Mo)			106.3		%		80-120	03-JUL-18
Nickel (Ni)			113.4		%		80-120	03-JUL-18
Selenium (Se)			115.9		%		80-120	03-JUL-18
Silver (Ag)			105.7		%		80-120	03-JUL-18
Thallium (TI)			108.8		%		80-120	03-JUL-18
Uranium (U)			114.1		%		80-120	03-JUL-18
Vanadium (V)			117.1		%		80-120	03-JUL-18
Zinc (Zn)			110.5		%		80-120	03-JUL-18
WG2812092-1 MB								
Antimony (Sb)			<0.10		mg/kg		0.1	03-JUL-18
Arsenic (As)			<0.10		mg/kg		0.1	03-JUL-18
Barium (Ba)			<0.50		mg/kg		0.5	03-JUL-18
Beryllium (Be)			<0.10		mg/kg		0.1	03-JUL-18
Boron (B)			<5.0		mg/kg		5	03-JUL-18
Cadmium (Cd)			<0.020		mg/kg		0.02	03-JUL-18



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Client: Soil Mat Engineers & Consulting Ltd. (Hamilton)

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Test	Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
MET-200.2-CCMS-WT	Soil							
Batch R4111909 WG2812092-1 MB Chromium (Cr)			<0.50		mg/kg		0.5	03-JUL-18
Cobalt (Co)			<0.10		mg/kg		0.1	03-JUL-18
Copper (Cu)			<0.50		mg/kg		0.5	03-JUL-18
Lead (Pb)			<0.50		mg/kg		0.5	03-JUL-18
Molybdenum (Mo)			<0.10		mg/kg		0.1	03-JUL-18
Nickel (Ni)			<0.50		mg/kg		0.5	03-JUL-18
Selenium (Se)			<0.20		mg/kg		0.2	03-JUL-18
Silver (Ag)			<0.10		mg/kg		0.1	03-JUL-18
Thallium (TI)			<0.050		mg/kg		0.05	03-JUL-18
Uranium (U)			<0.050		mg/kg		0.05	03-JUL-18
Vanadium (V)			<0.20		mg/kg		0.2	03-JUL-18
Zinc (Zn)			<2.0		mg/kg		2	03-JUL-18
Batch R4111915								
WG2810978-2 CRM Antimony (Sb)		WT-CANMET-	<b>FILL1</b> 103.0		%		70-130	03-JUL-18
Arsenic (As)			110.3		%		70-130	03-JUL-18
Barium (Ba)			110.1		%		70-130	03-JUL-18
Beryllium (Be)			97.3		%		70-130	03-JUL-18
Boron (B)			5.4		mg/kg		0-8.2	03-JUL-18
Cadmium (Cd)			105.7		%		70-130	03-JUL-18
Chromium (Cr)			107.9		%		70-130	03-JUL-18
Cobalt (Co)			108.6		%		70-130	03-JUL-18
Copper (Cu)			110.3		%		70-130	03-JUL-18
Lead (Pb)			104.9		%		70-130	03-JUL-18
Molybdenum (Mo)			103.2		%		70-130	03-JUL-18
Nickel (Ni)			108.8		%		70-130	03-JUL-18
Selenium (Se)			0.35		mg/kg		0.11-0.51	03-JUL-18
Silver (Ag)			0.24		mg/kg		0.13-0.33	03-JUL-18
Thallium (TI)			0.128		mg/kg		0.077-0.18	03-JUL-18
Uranium (U)			105.9		%		70-130	03-JUL-18
Vanadium (V)			107.1		%		70-130	03-JUL-18
Zinc (Zn)			109.4		%		70-130	03-JUL-18
WG2810978-6 DUP Antimony (Sb)		<b>WG2810978-5</b> 0.31	0.38		ug/g	21	30	03-JUL-18



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Client: Soil Mat Engineers & Consulting Ltd. (Hamilton)

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Test	Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
MET-200.2-CCMS-WT	Soil							
Batch R4111915								
WG2810978-6 DUP		WG2810978-5	4.00					
Arsenic (As)		1.59	1.92		ug/g	19	30	03-JUL-18
Barium (Ba)		20.6	23.7		ug/g	14	40	03-JUL-18
Beryllium (Be)		0.13	0.16		ug/g	25	30	03-JUL-18
Boron (B)		<5.0	<5.0	RPD-NA	ug/g	N/A	30	03-JUL-18
Cadmium (Cd)		0.084	0.096		ug/g	13	30	03-JUL-18
Chromium (Cr)		6.58	8.15		ug/g	21	30	03-JUL-18
Cobalt (Co)		2.31	2.79		ug/g	19	30	03-JUL-18
Copper (Cu)		7.96	9.60		ug/g	19	30	03-JUL-18
Lead (Pb)		21.3	23.0		ug/g	7.4	40	03-JUL-18
Molybdenum (Mo)		0.73	0.83		ug/g	13	40	03-JUL-18
Nickel (Ni)		4.48	5.61		ug/g	22	30	03-JUL-18
Selenium (Se)		<0.20	<0.20	RPD-NA	ug/g	N/A	30	03-JUL-18
Silver (Ag)		<0.10	<0.10	RPD-NA	ug/g	N/A	40	03-JUL-18
Thallium (TI)		< 0.050	<0.050	RPD-NA	ug/g	N/A	30	03-JUL-18
Uranium (U)		0.292	0.322		ug/g	9.7	30	03-JUL-18
Vanadium (V)		13.9	16.4		ug/g	17	30	03-JUL-18
Zinc (Zn)		32.1	40.3		ug/g	23	30	03-JUL-18
WG2810978-4 LCS								
Antimony (Sb)			103.7		%		80-120	03-JUL-18
Arsenic (As)			106.4		%		80-120	03-JUL-18
Barium (Ba)			107.5		%		80-120	03-JUL-18
Beryllium (Be)			97.4		%		80-120	03-JUL-18
Boron (B)			88.7		%		80-120	03-JUL-18
Cadmium (Cd)			104.8		%		80-120	03-JUL-18
Chromium (Cr)			106.9		%		80-120	03-JUL-18
Cobalt (Co)			107.0		%		80-120	03-JUL-18
Copper (Cu)			106.9		%		80-120	03-JUL-18
Lead (Pb)			106.8		%		80-120	03-JUL-18
Molybdenum (Mo)			100.8		%		80-120	03-JUL-18
Nickel (Ni)			107.3		%		80-120	03-JUL-18
Selenium (Se)			105.1		%		80-120	03-JUL-18
Silver (Ag)			101.3		%		80-120	03-JUL-18
Thallium (TI)			103.9		%		80-120	03-JUL-18



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Client: Soil Mat Engineers & Consulting Ltd. (Hamilton)

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Test	Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
MET-200.2-CCMS-WT	Soil							
Batch R4111915								
WG2810978-4 LCS Uranium (U)			106.9		%		80-120	00       40
Vanadium (V)			110.6		%		80-120	03-JUL-18 03-JUL-18
Zinc (Zn)			103.6		%		80-120	03-JUL-18
WG2810978-1 MB			100.0		70		00-120	03-JUL-16
Antimony (Sb)		<0.10 n		mg/kg		0.1	03-JUL-18	
Arsenic (As)			<0.10		mg/kg		0.1	03-JUL-18
Barium (Ba)			1.05	В	mg/kg		0.5	03-JUL-18
Beryllium (Be)			<0.10		mg/kg		0.1	03-JUL-18
Boron (B)			<5.0		mg/kg		5	03-JUL-18
Cadmium (Cd)			<0.020		mg/kg		0.02	03-JUL-18
Chromium (Cr)			<0.50		mg/kg		0.5	03-JUL-18
Cobalt (Co)			<0.10		mg/kg		0.1	03-JUL-18
Copper (Cu)			<0.50		mg/kg		0.5	03-JUL-18
Lead (Pb)			<0.50		mg/kg		0.5	03-JUL-18
Molybdenum (Mo)			<0.10		mg/kg		0.1	03-JUL-18
Nickel (Ni)			<0.50		mg/kg		0.5	03-JUL-18
Selenium (Se)			<0.20		mg/kg		0.2	03-JUL-18
Silver (Ag)			<0.10		mg/kg		0.1	03-JUL-18
Thallium (TI)			<0.050		mg/kg		0.05	03-JUL-18
Uranium (U)			<0.050		mg/kg		0.05	03-JUL-18
Vanadium (V)			<0.20		mg/kg		0.2	03-JUL-18
Zinc (Zn)			<2.0		mg/kg		2	03-JUL-18
MOISTURE-WT	Soil							
Batch R4102688								
<b>WG2810111-3 DUP</b> % Moisture		L2120219-9	45.0		%	0.7	00	
		15.2	15.3		70	0.7	20	29-JUN-18
WG2810111-2 LCS % Moisture			99.5		%		90-110	29-JUN-18
<b>WG2810111-1 MB</b> % Moisture			<0.10		%		0.1	29-JUN-18
Batch R4108989								
<b>WG2810565-3 DUP</b> % Moisture		<b>L2121208-1</b> 23.2 22.6			%	2.3	20	30-JUN-18
WG2810565-2 LCS % Moisture			99.97		%		90-110	30-JUN-18



Workorder: L2120222 Report Date: 05-JUL-18 Page 11 of 13

Client: Soil Mat Engineers & Consulting Ltd. (Hamilton)

130 Lancing Drive Hamilton ON L8W 3A1

Test	Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
MOISTURE-WT	Soil							
Batch R4108989 WG2810565-1 MB % Moisture			<0.10		%		0.1	30-JUN-18
Batch R4109014 WG2810417-3 DUP % Moisture		<b>L2121054-7</b> 10.6	10.2		%	4.0	20	30-JUN-18
<b>WG2810417-2 LCS</b> % Moisture			99.99		%		90-110	30-JUN-18
<b>WG2810417-1 MB</b> % Moisture			<0.10		%		0.1	30-JUN-18
PH-WT	Soil							
Batch R4104387								
<b>WG2809820-1 DUP</b> pH		<b>L2120222-4</b> 7.46	7.45	J	pH units	0.01	0.3	29-JUN-18
<b>WG2810503-1 LCS</b> pH			6.95		pH units		6.9-7.1	29-JUN-18
Batch R4105748								
<b>WG2810007-1 DUP</b> pH		<b>L2120249-8</b> 7.72	7.75	J	pH units	0.03	0.3	29-JUN-18
<b>WG2810508-1 LCS</b> pH			6.94		pH units		6.9-7.1	29-JUN-18
SAR-R511-WT	Soil							
Batch R4112111 WG2812107-4 DUP Calcium (Ca)		<b>WG2812107-3</b> 4.2	3.8		mg/L	10	30	03-JUL-18
Sodium (Na)		9.1	10.7		mg/L	16	30	03-JUL-18
Magnesium (Mg)		<1.0	<1.0	RPD-NA	mg/L	N/A	30	03-JUL-18
WG2812107-2 IRM		WT SAR2			_			
Calcium (Ca)			111.0		%		70-130	03-JUL-18
Sodium (Na)			96.0		%		70-130	03-JUL-18
Magnesium (Mg)			109.3		%		70-130	03-JUL-18
<b>WG2812107-1 MB</b> Calcium (Ca)			<1.0		mg/L		1	03-JUL-18
Sodium (Na)			<1.0		mg/L		1	03-JUL-18
Magnesium (Mg)			<1.0		mg/L		1	03-JUL-18



Workorder: L2120222 Report Date: 05-JUL-18 Page 12 of 13

Client: Soil Mat Engineers & Consulting Ltd. (Hamilton)

130 Lancing Drive Hamilton ON L8W 3A1

Test	Matrix	Reference	Result	Qualifier Units		RPD	Limit	Analyzed
SAR-R511-WT	Soil							
Batch R4112338	3							
WG2811033-4 DUP		WG2811033-	3					
Calcium (Ca)		7.1	7.7		mg/L	8.4	30	04-JUL-18
Sodium (Na)		353	366		mg/L	3.7	30	04-JUL-18
Magnesium (Mg)		1.1	1.9	J	mg/L	0.8	2	04-JUL-18
WG2811033-2 IRM		WT SAR2						
Calcium (Ca)			96.3		%		70-130	03-JUL-18
Sodium (Na)			88.1		%		70-130	03-JUL-18
Magnesium (Mg)			92.4		%		70-130	03-JUL-18
WG2811033-1 MB								
Calcium (Ca)			<1.0		mg/L		1	03-JUL-18
Sodium (Na)			<1.0		mg/L		1	03-JUL-18
Magnesium (Mg)			<1.0		mg/L		1	03-JUL-18

Report Date: 05-JUL-18 Workorder: L2120222

Soil Mat Engineers & Consulting Ltd. (Hamilton) Client:

130 Lancing Drive Hamilton ON L8W 3A1

Contact: Kyle Richardson

#### Legend:

CCV

CVS

Limit	ALS Control Limit (Data Quality Objectives)
DUP	Duplicate
RPD	Relative Percent Difference
N/A	Not Available
LCS	Laboratory Control Sample
SRM	Standard Reference Material
MS	Matrix Spike
MSD	Matrix Spike Duplicate
ADE	Average Desorption Efficiency
MB	Method Blank
IRM	Internal Reference Material
CRM	Certified Reference Material

Continuing Calibration Verification

Calibration Verification Standard LCSD Laboratory Control Sample Duplicate

#### **Sample Parameter Qualifier Definitions:**

Qualifier	Description
В	Method Blank exceeds ALS DQO. Associated sample results which are < Limit of Reporting or > 5 times blank level are considered reliable.
J	Duplicate results and limits are expressed in terms of absolute difference.
RPD-NA	Relative Percent Difference Not Available due to result(s) being less than detection limit.

#### **Hold Time Exceedances:**

All test results reported with this submission were conducted within ALS recommended hold times.

ALS recommended hold times may vary by province. They are assigned to meet known provincial and/or federal government requirements. In the absence of regulatory hold times, ALS establishes recommendations based on guidelines published by the US EPA, APHA Standard Methods, or Environment Canada (where available). For more information, please contact ALS.

The ALS Quality Control Report is provided to ALS clients upon request. ALS includes comprehensive QC checks with every analysis to ensure our high standards of quality are met. Each QC result has a known or expected target value, which is compared against predetermined data quality objectives to provide confidence in the accuracy of associated test results.

Please note that this report may contain QC results from anonymous Sample Duplicates and Matrix Spikes that do not originate from this Work Order.

Page 13 of 13

#### Chain of Custody (COC) / Analytical Request Form

Canada Toll Free: 1 800 668 9878

L2120222-COFC

📆 COC Number: 17 -

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Report To	Contact and company name below will appear on the final report Report Format / Distribution									<u> </u>	Contact y	our AM t	o confirm	all E&P	TATs (8	urcharge	s may	apply)	
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Contact:	Lyle Kichardson	^		QC) Report with Re			E	4 day [P	4-20%]		<u> </u>	Busines	s day [E1	I - 100%	[د				
Phone:	905-318-7440		Compare Result	s to Criteria on Report -			FIC RE	3 day [P	3-25%]		₩ Sa	me Day,	Weeken	d or Sta	itutory	holiday	[E2 -2C	00%	
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# ALS Environmental

## Chain of Custody (COC) / Analytical Request Form

Canada Toll Free: 1 800 668 9878

L2120222-COFC

COC Number: 17 -

Page  $\mathcal J$  of

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